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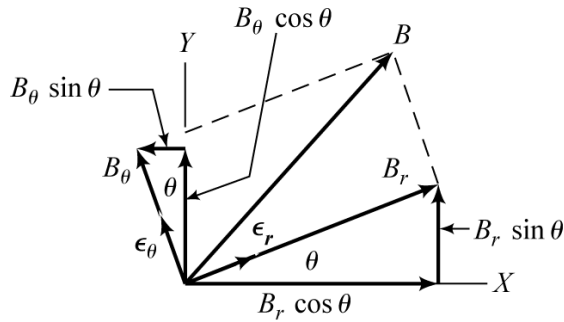
9  $V_{\max} = 5 + 5(3.33)^2 - 3.33^3$

11  $v_x = \dot{r}_x = -b\omega \sin\omega t \text{ m/sec}$  ,  $v_y = \dot{r}_y = b\omega \cos\omega t \text{ m/sec}$ ,

15

$$\begin{aligned} \ddot{\mathbf{r}} &= \ddot{r}\mathbf{e}_r + \dot{r}\dot{\theta}\mathbf{e}_\theta + (\dot{r}\dot{\theta} + r\ddot{\theta})\mathbf{e}_\theta - r\dot{\theta}^2\mathbf{e}_r \\ &= (\ddot{r} - r\dot{\theta}^2)\mathbf{e}_r + (r\ddot{\theta} + 2\dot{r}\dot{\theta})\mathbf{e}_\theta \\ &= a_r\mathbf{e}_r + a_\theta\mathbf{e}_\theta . \end{aligned} \tag{2.30}$$

16



19 2<sup>nd</sup> column, 9 lines down: Hence,  $\mathbf{v} = \mathbf{e}_r 20 \text{ m/sec}$ .

24 1<sup>st</sup> column, units

$$a_r = \ddot{r} - r\dot{\theta}^2 = -394.8 - 12.5 \times (-2.467)^2 = -470.9 \text{ mm/sec}^2 .$$

25 1<sup>st</sup> column

$$Y' = \frac{dY}{dX} = \frac{2A\pi}{L} \cos\left(\frac{2\pi X}{L}\right) = \frac{2 \times 100\pi}{2000} \times \cos\left(\frac{2\pi 750}{2000}\right) = -.222 \Rightarrow \beta = \tan^{-1}(-.222) = -12.52^\circ .$$

1<sup>st</sup> column, bottom, denominator

$$\frac{1}{\rho} = \frac{|Y''|}{[1+(Y')^2]^{3/2}} = \frac{6.98 \times 10^{-4}}{[1+(-.222)^2]^{3/2}} = 6.49 \times 10^{-4} \text{ m}^{-1} \Rightarrow \rho = 1540 \text{ m} ,$$

31

$$\dot{\boldsymbol{\omega}} = \hat{\boldsymbol{\omega}} \cdot \tag{2.72}$$

46

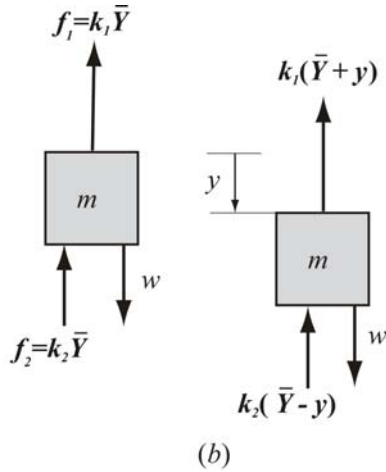
$$m \dot{Y}(t) - m \dot{Y}_0 = \int_0^t (-w) d\tau .$$

48

$$m\ddot{y} = \sum f_y = w - k_1(\bar{Y} + y) - k_2(\bar{Y} - y) = w - (k_1 + k_2)\bar{Y} - (k_1 + k_2)y = 0 - (k_1 + k_2)y$$

$$\therefore m\ddot{y} + (k_1 + k_2)y = 0 .$$

49 Fig. 3.6(b)



51 Caption, figure 3.7:  $Y(t)$  with  $k = 5.865 \times 10^6$ ; also second line, right column,  $k = 5.865 \times 10^6$

53 Proceeding to a time solution for  $m\ddot{Y} + c\dot{Y} + kY = w \dots$

54

$$\dot{Y} = e^{-\zeta\omega_n t} \omega_d (-A \sin\omega_d t + B \cos\omega_d t) - \zeta\omega_n e^{-\zeta\omega_n t} (A \cos\omega_d t + B \sin\omega_d t) .$$

56

$$x = x_h = e^{-\zeta\omega_n t} (A \cos\omega_d t + B \sin\omega_d t) , \tag{i}$$

59

$$\zeta = \frac{\delta}{[(2\pi)^2 + \delta^2]^{1/2}} = \frac{0.597}{\sqrt{4\pi^2 + .597^2}} = 0.095$$

60

$$m\ddot{Y} = \sum f_Y = -w - c(\dot{Y} - \dot{Y}_b) - k(Y - Y_b)$$

$$\therefore m\ddot{Y} + c\dot{Y} + kY = -w + kY_b + c\dot{Y}_b .$$

61  $\dot{x}$  in first row

$$m\ddot{x} = \sum f_x = k(x_b - x) + c(\dot{x}_b - \dot{x})$$

$$\therefore m\ddot{x} + c\dot{x} + kx = c\dot{x}_b + kx_b . \tag{i}$$

63 Misplaced decimal point and missing sec:  $c = 125.7Nsec/m$

64 In calculating  $\zeta$ , use 125.7, not 1257

71 1<sup>st</sup> column  $a = .25g = -\omega^2 A$

Denominator "377"

$$A = .25(9.81 \text{ m/sec}^2)/377.^2 = 1.726 \times 10^{-5} \text{ m} = .017 \text{ mm} .$$

86 The tension  $T_1$  can be eliminated by the operation: Eq.(3.84)  $\times \cos \theta$  - Eq.(3.83)  $\times \sin \theta$ , .. Also on pages 86 and 87 there are several typos where  $T_1$  is used incorrectly instead of  $T_1$  .

90

$$\begin{aligned} X_0 = X(0) = 0, & \quad Y_0 = Y(0) = 0 \\ \dot{X}(0) = \dot{X}_0 = v_0 \cos \alpha, & \quad \dot{Y}(0) = \dot{Y}_0 = v_0 \sin \alpha_0 , \end{aligned}$$

91 Second column, Example Problem 3.18

**Solution**

From Figure XP3.147

93

$$\frac{\dot{\theta}^2}{2} - \frac{\dot{\theta}_0^2}{2} = \frac{g}{r_0} \int_{\theta_0}^{\theta} \cos u \, du = \frac{g}{r_0} (\sin \theta - \sin \theta_0) , \quad (3.99)$$

97 1<sup>st</sup> column, last line ...Provided by Equation 3.793b ..  
2<sup>nd</sup> column

$$\begin{Bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{Bmatrix} = \begin{Bmatrix} x_2 \\ -\frac{g}{l} \sin x_1 - \frac{C_a}{ml} x_2^2 \operatorname{sgn} x_2 \end{Bmatrix} . \quad (3.113)$$

107

$$\begin{aligned} \Delta &= [(k_1 + k_2) - m_1 \omega^2] [(k_2 + k_3) - m_2 \omega^2] - k_2^2 \\ &= m_1 m_2 \omega^4 - [m_1(k_2 + k_3) + m_2(k_1 + k_2)] \omega^2 + (k_1 + k_2)(k_2 + k_3) - k_2^2 = 0 . \end{aligned} \quad (3.142)$$

108

$$(a_{i2}) = \begin{Bmatrix} a_{12} \\ a_{22} \end{Bmatrix} = \begin{Bmatrix} 1 \\ -.36603 \end{Bmatrix} .$$

109 Missing + sign in Eq. (3.153), and

$$\begin{bmatrix} (m_1 + m_2)l_1^2 & m_2 l_2 l_1 \\ m_2 l_1 l_2 & m_2 l_2^2 \end{bmatrix} \begin{Bmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{Bmatrix} + \begin{bmatrix} (w_1 + w_2)l_1 & 0 \\ 0 & w_2 l_2 \end{bmatrix} \begin{Bmatrix} \theta_1 \\ \theta_2 \end{Bmatrix} = 0 . \quad (3.138)$$

110

$$(a_{ii}) = \begin{Bmatrix} 1 \\ 1.2247 \end{Bmatrix}.$$

111

$$\begin{aligned} \begin{Bmatrix} q_{10} \\ q_{20} \end{Bmatrix} &= [A^*]^T [M] \begin{Bmatrix} x_{10} \\ x_{20} \end{Bmatrix} = \begin{bmatrix} .45970 & .62796 \\ .88807 & -.32506 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{Bmatrix} x_{10} \\ x_{20} \end{Bmatrix} \\ &= \begin{bmatrix} .45970 & 1.2559 \\ .88807 & -.65012 \end{bmatrix} \begin{Bmatrix} x_{10} \\ x_{20} \end{Bmatrix} = \begin{Bmatrix} .45970x_{10} + 1.2559x_{20} \\ .88807x_{10} - .65012x_{20} \end{Bmatrix}. \end{aligned}$$

$$\begin{Bmatrix} x_1(t) \\ x_2(t) \end{Bmatrix} = \begin{bmatrix} A^*_{11} & A^*_{12} \\ A^*_{21} & A^*_{22} \end{bmatrix} \begin{Bmatrix} q_1(t) \\ q_2(t) \end{Bmatrix} = q_1(t) \begin{Bmatrix} A^*_{11} \\ A^*_{21} \end{Bmatrix} + q_2(t) \begin{Bmatrix} A^*_{12} \\ A^*_{22} \end{Bmatrix}. \quad (3.155)$$

114

$$\ddot{q}_1 + 1.294\dot{q}_1 + 41.886q_1 = 0, \quad \ddot{q}_2 + 3.785\dot{q}_2 + 358.11q_2 = 0$$

$$\begin{Bmatrix} x_1 \\ x_2 \end{Bmatrix} = \begin{bmatrix} .07377 & .03500 \\ .04287 & -.09034 \end{bmatrix} \begin{Bmatrix} q_1 \\ q_2 \end{Bmatrix}. \quad (i)$$

115

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{Bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{Bmatrix} + \begin{bmatrix} (k_1+k_2) & -k_2 \\ -k_2 & (k_2+k_3) \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \end{Bmatrix} = \begin{Bmatrix} f_{1o} \\ f_{2o} \end{Bmatrix} \sin \omega t, \quad (3.158)$$

116

$$\begin{aligned} \begin{Bmatrix} \ddot{q}_1 + .6340 q_1 \\ \ddot{q}_2 + 2.336 q_2 \end{Bmatrix} &= \begin{bmatrix} .4597 & .6280 \\ .8881 & -.3251 \end{bmatrix} \begin{Bmatrix} f_{10} \\ f_{20} \end{Bmatrix} \sin \omega t \\ &= \begin{Bmatrix} .4597f_{10} + .6280f_{20} \\ .8881f_{10} - .3251f_{20} \end{Bmatrix} \sin \omega t. \end{aligned}$$

$$\begin{Bmatrix} x_1(\omega, t) \\ x_2(\omega, t) \end{Bmatrix}_{ss} = q_{1ss}(\omega, t) \begin{Bmatrix} .4597 \\ .6280 \end{Bmatrix} + q_{2ss}(\omega, t) \begin{Bmatrix} .8881 \\ -.3251 \end{Bmatrix} (m). \quad (3.160)$$

$$X_1 = \frac{f_{10} [ - m_2 \omega^2 + ( k_2 + k_3 ) ] + f_{20} k_1}{m_1 m_2 \omega^4 - [ m_1 ( k_2 + k_3 ) + m_2 ( k_1 + k_2 ) ] \omega^2 + ( k_1 + k_2 ) ( k_2 + k_3 ) - k_2^2}$$

$$X_2 = \frac{f_{10} k_2 + f_{20} [ ( k_1 + k_2 ) - m_1 \omega^2 ]}{m_1 m_2 \omega^4 - [ m_1 ( k_2 + k_3 ) + m_2 ( k_1 + k_2 ) ] \omega^2 + ( k_1 + k_2 ) ( k_2 + k_3 ) - k_2^2} .$$
(3.162)

$$[M] \{ -\omega^2 (x_{is}) \sin \omega t - \omega^2 (x_{ic}) \cos \omega t \} + [C] \{ \omega (x_{is}) \cos \omega t - (x_{ic}) \sin \omega t \}$$

$$+ [K] \{ (x_{is}) \sin \omega t + (x_{ic}) \cos \omega t \} = \{ f_{i0} \} \sin \omega t .$$

142 Problem 3.13.  $c_A = 6.0 \text{ lbsec/in}$

145  $\zeta \approx 0.0075$

150 3.51 (c) Normalize the eigenvectors ... diagonal matrix with of eigenvalues.

151

$$x_1(0) = x_2(0) = \dot{x}_1(0) = 0; \quad \dot{x}_2(0) = 1 \frac{\text{cm}}{\text{sec}}$$

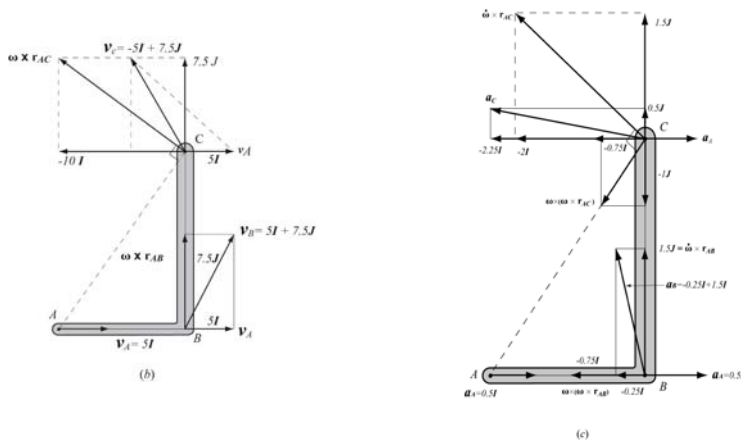
156 1<sup>st</sup> column, missing  $r$ :  $\mathbf{a}_A = \boldsymbol{\varepsilon}_0 r \ddot{\theta} - \boldsymbol{\varepsilon}_r r \dot{\theta}^2$

158

$$\mathbf{v}_C = \mathbf{v}_A + \boldsymbol{\omega} \times \mathbf{r}_{AC} = 5\mathbf{I} + .1\mathbf{K} \times (75\mathbf{I} + 100\mathbf{J}) = 5\mathbf{I} + 7.5\mathbf{J} - 10\mathbf{I} \text{ mm/sec}$$

159  $7.5 \mathbf{J}$  not  $7.5 \mathbf{I}$

XP4.1(b) &(c)



$$\mathbf{a}_B' = \mathbf{a}_O + \dot{\boldsymbol{\omega}} \times \mathbf{r}_{OB'} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{r}_{OB'}) = \mathbf{J} \mathbf{a}_O + (\mathbf{K} \dot{\theta} \times .2\mathbf{I}) + [\mathbf{K} \dot{\theta} \times (\mathbf{K} \dot{\theta} \times .2\mathbf{I})]$$

$$= \mathbf{J} \mathbf{a}_O + \mathbf{J} .2\ddot{\theta} - \mathbf{I} .2\dot{\theta}^2 = \mathbf{J} (\mathbf{a}_O + .2\ddot{\theta}) - \mathbf{I} .2\dot{\theta}^2 \text{ m/sec}^2$$

(iii)

$$(-.2\dot{\theta}^2 \mathbf{I} - .13\mathbf{J}) = (.2\dot{\theta}^2 \mathbf{I} + .13\mathbf{J}) + (\mathbf{K} \dot{\theta} \times .4\mathbf{I}) + [\mathbf{K} \dot{\theta} \times (\mathbf{K} \dot{\theta} \times .4\mathbf{I})]$$

$$= .2\dot{\theta}^2 \mathbf{I} + .13\mathbf{J} + .4\ddot{\theta} \mathbf{J} - .4\dot{\theta}^2 \mathbf{I} \text{ m/sec}^2$$

$$\begin{aligned} \mathbf{a}_o &= \mathbf{a}_{A'} + \dot{\boldsymbol{\omega}} \times \mathbf{r}_{A'o} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{r}_{A'o}) = (.2\dot{\theta}^2 \mathbf{I} + .13 \mathbf{J}) + (\mathbf{K}\ddot{\theta} \times .2\mathbf{I}) + [\mathbf{K}\dot{\theta} \times (\mathbf{K}\dot{\theta} \times .2\mathbf{I})] \\ &= .2\dot{\theta}^2 \mathbf{I} + .13 \mathbf{J} + .2\ddot{\theta} \mathbf{J} - .2\dot{\theta}^2 \mathbf{I} = (.13 + .2 \times -.65) \mathbf{J} = 0 \mathbf{J} \text{ m/sec}^2 \end{aligned}$$

$$\begin{aligned} \mathbf{a}_P &= \mathbf{a}_{A'} + \dot{\boldsymbol{\omega}} \times \mathbf{r}_{A'P} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{r}_{A'P}) \\ &= (.2\dot{\theta}^2 \mathbf{I} + .13 \mathbf{J}) + \mathbf{K}\ddot{\theta} \times (.2\mathbf{I} + .2\mathbf{J}) + \mathbf{K}\dot{\theta} \times [\mathbf{K}\dot{\theta} \times (.2\mathbf{I} + .2\mathbf{J})] \\ &= .2\dot{\theta}^2 \mathbf{I} + .13 \mathbf{J} + .2\ddot{\theta}(\mathbf{J} - \mathbf{I}) - .2\dot{\theta}^2(\mathbf{I} + \mathbf{J}) = -.2\ddot{\theta} \mathbf{I} + (.13 + .2\ddot{\theta} - .2\dot{\theta}^2) \mathbf{J} \\ &= (-.2 \times -.65) \mathbf{I} + [.13 + (.2 \times -.65) - .2 \times 1.5^2] \mathbf{J} = 0.13 \mathbf{I} - 0.45 \mathbf{J} \text{ m/sec}^2 . \end{aligned}$$

162

$$\begin{aligned} \dot{X} &= r\dot{\theta} + r\dot{\theta}(-1) = 0, \quad \dot{Y} = -r\dot{\theta}(0) = 0 \\ \ddot{X} &= r\ddot{\theta} + r\ddot{\theta}(-1) - r\dot{\theta}^2(0) = 0, \quad \ddot{Y} = -r\ddot{\theta}(0) - r\dot{\theta}^2(-1) = r\dot{\theta}^2 . \end{aligned} \tag{4.11}$$

164

$$\mathbf{a}_C = (I\mathbf{a}_{CX} + J\mathbf{a}_{CY}) = I\ddot{X}_o + (-\mathbf{K}\ddot{\theta} \times -Jr) - \mathbf{K}\dot{\theta} \times (-\mathbf{K}\dot{\theta} \times -Jr)$$

$$\mathbf{a}_D = Ir\ddot{\theta} + (-\mathbf{K}\ddot{\theta} \times -Ir) - \mathbf{K}\dot{\theta} \times (-\mathbf{K}\dot{\theta} \times -Ir) = I(r\ddot{\theta} + r\dot{\theta}^2) + Jr\ddot{\theta} .$$

166

$$\mathbf{v}_C = \mathbf{v}_A + \boldsymbol{\omega} \times \mathbf{r}_{AC} \text{ or,}$$

$$-I(1.25 \text{ m/sec}) = 0 + \mathbf{K}\dot{\theta}(\text{rad/sec}) \times -0.5 \text{ m} \mathbf{J} = I0.5\dot{\theta}(\text{m/sec}) \tag{i}$$

$$\therefore \dot{\theta} = -1.25/.5 = -2.5 \text{ rad/sec}, \quad \boldsymbol{\omega} = -\mathbf{K}2.5 \text{ rad/sec}$$

167

$$\mathbf{I}: 1 = (a_{oX} + \ddot{\theta}) \Rightarrow a_{oX} = (1 - 2) = -1 \text{ m/sec}^2$$

$$\mathbf{J}: a_{CY} = \dot{\theta}^2 = (-2.5)^2 \text{ m/sec}^2 = 6.25 \text{ m/sec}^2 . \tag{iii}$$

Note that  $a_{AY} = r_{oA} \dot{\theta}^2 = 0.5 \times (-2.5)^2 = 3.125 \text{ m/sec}^2$ .

169

The wheel that rolled without slipping in the preceding section provides an appropriate “thought model” for the present topic of planar mechanisms. The wheel example had the following two characteristics that carry apply here:

$$\begin{bmatrix} 1 & \sin\phi \\ 0 & \cos\phi \end{bmatrix} \begin{Bmatrix} \dot{X}_P \\ L_2 \dot{\phi} \end{Bmatrix} = L_1 \boldsymbol{\omega} \begin{Bmatrix} -\sin\theta \\ \cos\theta \end{Bmatrix} . \tag{4.18b}$$

$$l_1 \cos \theta + l_2 \cos \varphi = X_p, \quad l_1 \sin \theta - l_2 \sin \varphi = 0. \quad (4.20a)$$

175 Equations (4.21) define the position vectors of this equation. Using the right-hand rule, the angular velocity vectors are defined as  $\boldsymbol{\omega}_1 = \mathbf{K}\dot{\alpha}$ ,  $\boldsymbol{\omega}_2 = \mathbf{K}\dot{\beta}$ , and  $\boldsymbol{\omega}_3 = -\mathbf{K}\dot{\gamma}$ .

$$\mathbf{a}_D + \dot{\boldsymbol{\omega}}_3 \times \mathbf{r}_{DC} + \boldsymbol{\omega}_3 \times (\boldsymbol{\omega}_3 \times \mathbf{r}_{BC}) = \mathbf{a}_A + \dot{\boldsymbol{\omega}}_1 \times \mathbf{r}_{AB} + \boldsymbol{\omega}_1 \times (\boldsymbol{\omega}_1 \times \mathbf{r}_{AB}) + \dot{\boldsymbol{\omega}}_2 \times \mathbf{r}_{BC} + \boldsymbol{\omega}_2 \times (\boldsymbol{\omega}_2 \times \mathbf{r}_{BC}).$$

Noting that  $\mathbf{a}_D$  and  $\mathbf{a}_A$  are zero, and substituting  $\dot{\boldsymbol{\omega}}_1 = \mathbf{K}\ddot{\alpha}$ ,  $\dot{\boldsymbol{\omega}}_2 = \mathbf{K}\ddot{\beta}$ , and  $\dot{\boldsymbol{\omega}}_3 = -\mathbf{K}\ddot{\gamma}$

$$\begin{aligned} & -\mathbf{K}\ddot{\gamma} \times l_3(-I \cos \gamma + J \sin \gamma) - \mathbf{K}\dot{\gamma} \times [-\mathbf{K}\dot{\gamma} \times l_3(-I \cos \gamma + J \sin \gamma)] = \\ & \mathbf{K}\ddot{\alpha} \times l_1(I \cos \alpha + J \sin \alpha) + \mathbf{K}\dot{\alpha} \times [\mathbf{K}\dot{\alpha} \times l_1(I \cos \alpha + J \sin \alpha)] \\ & + \mathbf{K}\ddot{\beta} \times l_2(I \cos \beta + J \sin \beta) + \mathbf{K}\dot{\beta} \times [\mathbf{K}\dot{\beta} \times l_2(I \cos \beta + J \sin \beta)]. \end{aligned}$$

176

$$-l_1 \cos \alpha + l_2 \sin \beta + l_3 \cos \gamma = a \Rightarrow l_2 \sin \beta + l_3 \cos \gamma = a + l_1 \cos \alpha = h_1(\alpha)$$

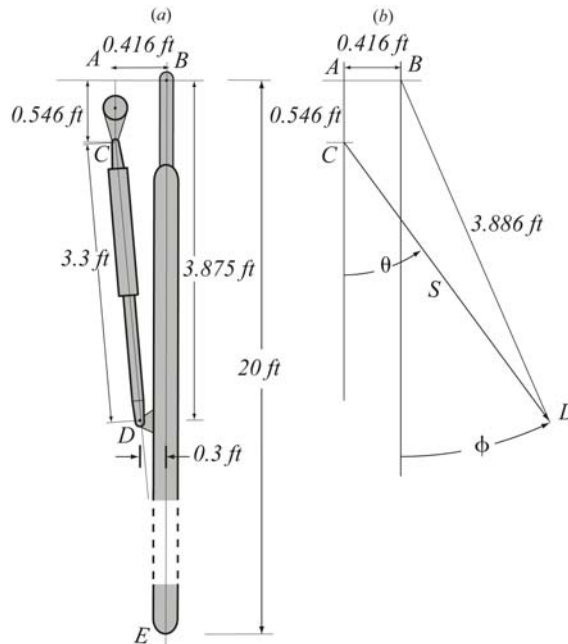
$$l_1 \sin \alpha + l_2 \cos \beta - l_3 \sin \gamma = b \Rightarrow l_2 \cos \beta - l_3 \sin \gamma = b - l_1 \sin \alpha = h_2(\alpha),$$

(i)

177

$$\begin{bmatrix} \cos \beta & -\sin \gamma \\ \sin \beta & \cos \gamma \end{bmatrix} \begin{Bmatrix} l_2 \ddot{\beta} \\ l_3 \ddot{\gamma} \end{Bmatrix} = \begin{Bmatrix} g_1 \\ g_2 \end{Bmatrix}.$$

182 XP4.6 (a) &amp; (b)



190 Consistent with the problem 4.30 figure, the problem statement should be referring to bar  $BC$  not  $BA$  .

196  $\rho = i\mathbf{x} + j\mathbf{y} + k\mathbf{z}$

202 Missing  $\times$

$$\rho \times \dot{\mathbf{r}} = (\rho \times \ddot{\mathbf{R}}_o) + \rho \times (\dot{\omega} \times \rho) + \rho \times [\omega \times (\omega \times \rho)] .$$

203 Missing =

$$m \mathbf{b}_{og} = m(i b_{ogx} + j b_{ogy} + k b_{ogz}) = \int_V \rho \gamma dx dy dz = \int_m \rho dm , \quad (5.2)$$

$$\omega \times \rho = k \dot{\theta} \times (ix + jy + kz) = \dot{\theta} (j x - i y) , \quad (5.30)$$

204 Think about driving a nail through point  $o$  in figure 5-63 5.8

207  $Work_{n.c.} = (T + V) - (T_0 + V_0) \dots$

208

$$I_o \ddot{\theta} = T_{c2} r - T_{c1} r = r(w_2 - m_2 r \ddot{\theta}) - r(w_1 + m_1 r \ddot{\theta}) \quad (5.50)$$

$$y_1 + y_2 + c = \text{cord length} \Rightarrow \ddot{y}_1 = -\ddot{y}_2 .$$

209

$$T = I_o \frac{\dot{\theta}^2}{2} + m_1 \frac{(-r\dot{\theta})^2}{2} + m_2 \frac{(r\dot{\theta})^2}{2} = (I_o + m_1 r^2 + m_2 r^2) \frac{\dot{\theta}^2}{2}$$

210

$$T + V = T_0 + V_0 \Rightarrow \frac{I_o \dot{\theta}^2}{2} + \frac{m \dot{x}^2}{2} - mg(\bar{x} + \delta x) = T_0 + V_0 .$$

211 Figure 5.16-a 5.16a illustrates a compound pendulum consisting of a uniform ...

212 (l not 1)

$$I_o \ddot{\theta} = \Sigma M_o = -w \frac{l}{2} \sin \theta , \quad I_o = \frac{ml^2}{3} \quad (5.59)$$

The degree sign is missing in  $(\theta \leq \text{about } 15^\circ = .262 \text{ radians})$

214 (l not 1)

$$V = -w \frac{l}{2} \cos \theta . \quad (5.70)$$

215 Moving to Task b, the immediate choice ... (Not italicised)

217 Adding this resistance moment to the moments on the right of Equation (5.33)-(5.59) gives (l not 1)



$$\frac{ml^2}{3} \ddot{\theta} = -w \frac{l}{2} \sin \theta - C_d \dot{\theta} , \quad (5.71)$$

218 **l not 1**

$$\begin{aligned} \Sigma M_o = I_o \ddot{\theta} &= -w \frac{l}{2} \sin \theta - k \delta_s \cos \beta \times l \cos \theta - k \delta_s \sin \beta \times l \sin \theta \\ &= -w \frac{l}{2} \sin \theta - k \delta_s l \cos(\theta - \beta) \end{aligned} \quad (5.76)$$

219 For the small displacement of the spring, starting with  $T+V=T_0+V_0$ , the EOM is.. ( $T_0+V_0$ )

222 **l not 1**

$$\begin{aligned} \Sigma M_o = I_o \delta \ddot{\theta} &= -w \frac{l}{2} \sin(\bar{\theta} + \delta\theta) + \frac{2l}{3} k_1 (\delta_1 - \frac{2l}{3} \theta) + \frac{2l}{3} k_2 (\delta_2 - \frac{2l}{3} \theta) \\ &= -w \frac{l}{2} (\sin \bar{\theta} + \cos \bar{\theta} \delta\theta) + \frac{2l}{3} k_1 \delta_1 + \frac{2l}{3} k_2 \delta_2 - (\frac{2l}{3})^2 (k_1 + k_2) \delta\theta \\ &= (-w \frac{l}{2} \sin \bar{\theta} + \frac{2l}{3} k_1 \delta_1 + \frac{2l}{3} k_2 \delta_2) - w \frac{l}{2} \cos \bar{\theta} \delta\theta - (\frac{2l}{3})^2 (k_1 + k_2) \delta\theta , \end{aligned}$$

$$\frac{ml^2}{3} \delta \ddot{\theta} + [(\frac{2l}{3})^2 (k_1 + k_2) + w \frac{l}{2} \cos \bar{\theta}] \delta\theta = 0 = -w \frac{l}{2} \sin \bar{\theta} + \frac{2l}{3} k_1 \delta_1 + \frac{2l}{3} k_2 \delta_2 . \quad (5.85)$$

223 **(l not 1)**

$$\frac{ml^2}{3} \delta \ddot{\theta} + [(\frac{2l}{3})^2 (k_1 + k_2) + w \frac{l}{2} \cos \bar{\theta}] \delta\theta = 0 = -w \frac{l}{2} \sin \bar{\theta} + \frac{2l}{3} k_1 \delta_1 - \frac{2l}{3} k_2 \delta_2 . \quad (5.88)$$

$$\begin{aligned} \Sigma M_o = I_o \delta \ddot{\theta} &= -w \frac{l}{2} \sin(\bar{\theta} + \delta\theta) + k_x (\delta_x - l \delta\theta \cos \bar{\theta}) \times l \cos(\bar{\theta} + \delta\theta) \\ &\quad + k_y (\delta_y - l \delta\theta \sin \bar{\theta}) \times l \sin(\bar{\theta} + \delta\theta) \end{aligned}$$

248

$$\int_{\beta_0}^{\pi/2} 2\bar{f} l \cos \beta d\beta = 2\bar{f} l (1 - \sin \beta_0) = \frac{m l^2}{3} \dot{\beta}^2 (\beta = \pi/2) + 2wl(1 - \sin \beta_0) + 2kl^2(1 - \sin \beta_0)^2 ,$$

251

$$T = 2 \times \frac{I_O \dot{\theta}^2}{2} + 2 \times \left[ \frac{I_g \dot{\theta}^2}{2} + \frac{m}{2} (\dot{X}_g^2 + \dot{Y}_g^2) \right] + \frac{m}{2} (l\dot{\theta})^2 + \left( \frac{I_B \dot{\beta}^2}{2} + \frac{M \dot{X}_r^2}{2} \right). \quad (5.191)$$

258

$$\begin{Bmatrix} \bar{f}_X \\ \bar{M}_Y \end{Bmatrix} = -[k_{ZZ}] \begin{Bmatrix} R_X \\ \beta_Y \end{Bmatrix} = - \begin{bmatrix} 12EI_a/l^3 & -6EI_a/l^2 \\ -6EI_a/l^2 & 4EI_a/l \end{bmatrix} \begin{Bmatrix} R_X \\ \beta_Y \end{Bmatrix}. \quad (5.214)$$

260 Denominator  $(6m)^3$

$$k_c = \frac{12EI_{al}}{l^3} = \frac{12(1.75 \times 10^6)Nm^2}{(6m)^3} = 97200 \frac{N}{m}$$

296 Problem 5.26 Determine the angular velocity...

300 Problem 5.45 The bar assembly shown in Figure P5.45 is being pulled upward by a vertical force  $F$  at  $B$ . The spring connecting  $O$  and  $A$  is undeflected when the roller at  $B$  is resting on  $O$ .

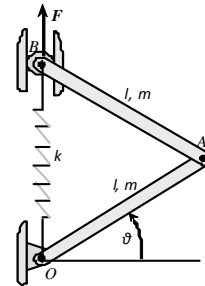


Figure P5.45

307 Problem 5.71

(c) For the data provided below, obtain the eigenvalues, normalized eigenvectors, and natural frequencies of the system.

Problem 5.74

..... A small mass roller at  $B$  (negligible mass and inertia) supports the right end of bar  $AB$ .

310 Problem 5.85

..... Links  $OB$ 's mass center is located at distance  $\bar{r}$  from  $O$ .

Problem 5.86

..... The mass center of wheel  $B$  is at  $O_2$  and has a radius of gyration of  $k_{2g}$  about point  $O_2$ . Pin  $C$  is fixed to disk  $A$  and is located a distance  $r$  from the pivot  $O_1$ . Disk  $A$ 's mass center is located at  $\bar{r}$  from point  $O_1$ . Disk  $A$  has mass  $m_1$  and a radius of gyration of  $k_{1g}$  about point  $O_1$ .

311 Problem 5.90

(a) Select coordinates and state the kinematic constraint relationships.

312 Problem 5.91

..... and link  $BC$  is a uniform bar of mass  $M$ .

Problem 5.92

(a) Select coordinates and state the kinematic constraint relationships.

NOTE: Original problem had torque  $T$  acting on the disc at  $O$ , and appears in answer.

313 Matrix algebra requires that the number of rows columns in the first matrix equal the number of columns rows in the second matrix.

$$\begin{aligned}
 (\ddot{q})_i + [\Lambda](q_i) = (Q_i) &= [A^*]^T (f_i) = \begin{bmatrix} A^*_{11} & A^*_{21} \\ A^*_{12} & A^*_{22} \end{bmatrix} \begin{Bmatrix} f_1 \\ f_2 \end{Bmatrix} \\
 &= \begin{Bmatrix} A^*_{11} f_1 + A^*_{21} f_2 \\ A^*_{12} f_1 + A^*_{22} f_2 \end{Bmatrix}.
 \end{aligned}
 \tag{3.153}$$

330 In the last figure for problem 2.7.  $a_n = 0.00996$   
 333 1<sup>st</sup> column

$$\begin{Bmatrix} a_t \\ a_n \end{Bmatrix} = \begin{Bmatrix} 683 \\ 1267 \end{Bmatrix} \text{ m/sec}^2$$

2<sup>nd</sup> column

$$\begin{Bmatrix} a_r \\ a_\theta \end{Bmatrix} = \begin{Bmatrix} -1695 \\ -242 \end{Bmatrix} \times 10^3 \text{ mm/sec}^2$$

335 Bottom of the page, 2<sup>nd</sup> column  $\theta = 323^\circ$   
 $\beta = 333^\circ$

339 Answer, problem 2.20

$$\begin{Bmatrix} v_r \\ v_\theta \end{Bmatrix} = \begin{Bmatrix} -5.78 \\ -39.6 \end{Bmatrix}, \quad \begin{Bmatrix} a_r \\ a_\theta \end{Bmatrix} = \begin{Bmatrix} 29.68 \\ -4.25 \end{Bmatrix}$$

342  $\ddot{X} + 5.02\dot{X} + 1000X = 0.03333t^2 - 0.1t$

344 3.27(b),  $a = 0.913$  mm

345 answer, missing 2 in denominator

$$\zeta = \frac{c_b}{2\sqrt{(k_B + 9k_C)(m_B + 9m_C)}}$$

346

$$(m_b + 9m_c)\ddot{X} + c_b\dot{X} + (k_B + 9k_C)X = w_B - 3w_C$$

350 problem 4.21: (a)  $v_B = -344.4 \text{ in/s}$  (b)  $a_B = -212087 \text{ in/s}^2$

353 4.35

$$\dot{S} = \frac{-l_1 \dot{\theta} \sin(\theta + \varphi)}{\cos \varphi}, \quad \dot{\varphi} = \frac{-l_1 \dot{\theta} \cos \theta}{l_2 \cos \varphi}$$

$$4.37c \quad \mathbf{v}_C = -\mathbf{I}(r\dot{\theta}\sin\theta + L\dot{\phi}\sin\phi) - \mathbf{J}(r\dot{\theta}\cos\theta + L\dot{\phi}\cos\phi)$$

$$357 \quad 5.26 \quad \ddot{\theta} = \frac{3}{2L}(a_o \cos\theta + g \sin\theta)$$

$$359 \quad 5.45 \quad \left(\frac{2}{3} + 2\cos^2\theta\right)ml\ddot{\theta} - ml\dot{\theta}^2 \sin 2\theta + 2mg \cos\theta + 2kl \sin 2\theta = 2FL \cos\theta$$