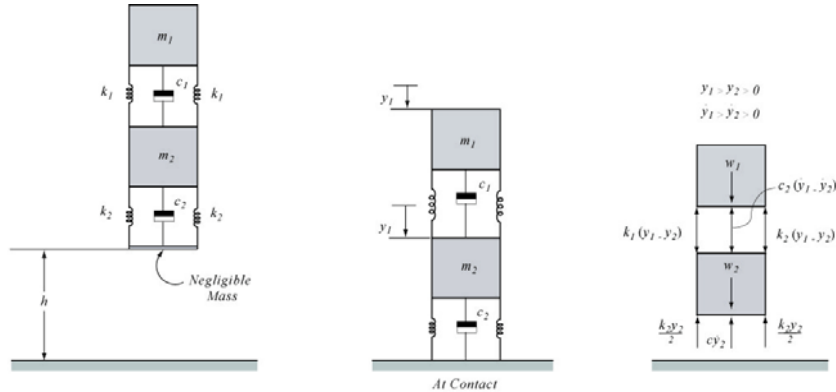


## Lecture 17. MORE TRANSIENT MOTION USING MODAL COORDINATES

### Example



At the left is an assembly that is released from a height  $h = 2\text{ft}$  above the ground. In the middle, the assembly has just contacted the ground. The subsequent positions of  $m_1$  and  $m_2$  are defined, respectively, by  $y_1$  and  $y_2$ . At the time of contact,  $y_1(0) = y_2(0) = 0$ , and  $\dot{y}_1(0) = \dot{y}_2(0) = v_0 = \sqrt{2gh} = \sqrt{2 \times 32.2 \times 2} = 11.35\text{ft/sec}$  ..

Engineering-analysis tasks:

- Draw free-body diagrams and derive the equations of motion.
- State the matrix equations of motion.

c. Solve for two cycles of motion for the lowest natural frequency.

**Equation of Motion from Free-body diagrams:**

$$\begin{aligned} m_1 \ddot{y}_1 &= \sum f_{y_1} = w_1 - k_1(y_1 - y_2) - c_1(\dot{y}_1 - \dot{y}_2) \\ m_2 \ddot{y}_2 &= \sum f_{y_2} = w_2 - k_2 y_2 - c_2 \dot{y}_2 + k_1(y_1 - y_2) + c_1(\dot{y}_1 - \dot{y}_2) . \end{aligned} \quad (1)$$

**Matrix Format:**

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{Bmatrix} \ddot{y}_1 \\ \ddot{y}_2 \end{Bmatrix} + \begin{bmatrix} c_1 & -c_1 \\ -c_1 & (c_1 + c_2) \end{bmatrix} \begin{Bmatrix} \dot{y}_1 \\ \dot{y}_2 \end{Bmatrix} + \begin{bmatrix} k_1 & -k_1 \\ -k_1 & (k_1 + k_2) \end{bmatrix} \begin{Bmatrix} y_1 \\ y_2 \end{Bmatrix} = \begin{Bmatrix} w_1 \\ w_2 \end{Bmatrix} . \quad (2)$$

**Equations for Modal Coordinates using Modal damping to account for internal damping**

$$(\ddot{q})_i + [2\zeta\omega_n](\dot{q}_i) + [\Lambda](q_i) = (Q_i) = [A^*]^T(f_i)$$

$$= \begin{bmatrix} A_{11}^* & A_{21}^* \\ A_{12}^* & A_{22}^* \end{bmatrix} \begin{Bmatrix} w_1 \\ w_2 \end{Bmatrix} = \begin{Bmatrix} A_{11}^* w_1 + A_{21}^* w_2 \\ A_{12}^* w_1 + A_{22}^* w_2 \end{Bmatrix} .$$

**Component modal differential equations:**

$$\begin{aligned}\ddot{q}_1 + 2\zeta_1 \omega_{n1} \dot{q}_1 + \omega_{n1}^2 q_1 &= Q_1 = A_{11}^* w_1 + A_{21}^* w_2 \\ \ddot{q}_2 + 2\zeta_2 \omega_{n2} \dot{q}_2 + \omega_{n2}^2 q_2 &= Q_2 = A_{12}^* w_1 + A_{22}^* w_2 .\end{aligned}\quad (3)$$

The homogeneous version of Eq.(3) is

$$\ddot{q}_{1h} + 2\zeta_1 \omega_{n1} \dot{q}_{1h} + \omega_{n1}^2 q_{1h} = 0 , \quad \ddot{q}_{2h} + 2\zeta_2 \omega_{n2} \dot{q}_{2h} + \omega_{n2}^2 q_{2h} = 0 ,$$

with solutions:

$$\begin{aligned}q_{1h}(t) &= e^{-\zeta_1 \omega_{n1} t} (A_1 \cos \omega_{d1} t + B_1 \sin \omega_{d1} t) \\ q_{2h}(t) &= e^{-\zeta_2 \omega_{n2} t} (A_2 \cos \omega_{d2} t + B_2 \sin \omega_{d2} t) .\end{aligned}$$

The particular solutions  $q_{1p}(t), q_{2p}(t)$  corresponding to Eq.(3) are

$$q_{1p} = (A_{11}^* w_1 + A_{21}^* w_2) / \omega_{n1}^2 , \quad q_{2p} = (A_{12}^* w_1 + A_{22}^* w_2) / \omega_{n2}^2 ,$$

yielding the complete modal-coordinate solutions

$$\begin{aligned}q_1(t) &= \frac{(A_{11}^* w_1 + A_{21}^* w_2)}{\omega_{n1}^2} + e^{-\zeta_1 \omega_{n1} t} (A_1 \cos \omega_{d1} t + B_1 \sin \omega_{d1} t) \\ q_2(t) &= \frac{(A_{12}^* w_1 + A_{22}^* w_2)}{\omega_{n2}^2} + e^{-\zeta_2 \omega_{n2} t} (A_2 \cos \omega_{d2} t + B_2 \sin \omega_{d2} t) .\end{aligned}$$

The constants  $A_i, B_i$  must be determined from the modal-coordinate initial conditions.

The modal-coordinate initial conditions are defined by

$$(q_0) = [A^*]^T [M] (y_0) .$$

Similarly, the modal-velocity initial conditions are defined by

$$(\dot{q}_0) = [A^*]^T [M] (\dot{y}_0) .$$

A previous undamped model had the physical parameters:

$$m_1 = 150 \text{ kg}, m_2 = 100 \text{ kg} , k_1 = k_2 = 1.5 \times 10^4 \text{ N/m},$$

yielding

$$[M] = \begin{bmatrix} 150 & 0 \\ 0 & 100 \end{bmatrix}, \quad [K] = \begin{bmatrix} 1.5 \times 10^4 & -1.5 \times 10^4 \\ -1.5 \times 10^4 & 3.0 \times 10^4 \end{bmatrix}$$

$$\{w_i\} = \begin{Bmatrix} 1457 \\ 981 \end{Bmatrix}.$$

The eigenvalues and natural frequencies are:

$$\omega_{n1}^2 = 41.886 \text{ sec}^{-2} \Rightarrow \omega_{n1} = 6.4720 \text{ sec}^{-1}$$

$$\omega_{n2}^2 = 358.11 \text{ sec}^{-2} \Rightarrow \omega_{n2} = 18.924 \text{ sec}^{-1}.$$

The matrix of normalized eigenvectors is

$$[A^*] = \begin{bmatrix} .073767 & .035002 \\ .042866 & -.090344 \end{bmatrix}.$$

From,

$$\ddot{q}_1 + 2\zeta_1 \omega_{n1} \dot{q}_1 + \omega_{n1}^2 q_1 = Q_1 = A_{11}^* w_1 + A_{21}^* w_2$$

$$\ddot{q}_2 + 2\zeta_2 \omega_{n2} \dot{q}_2 + \omega_{n2}^2 q_2 = Q_2 = A_{12}^* w_1 + A_{22}^* w_2 ,$$
(3)

the model (with 5% modal damping) is

$$\ddot{q}_1 + 6.47 \dot{q}_1 + 41.886 q_1 = 149.5$$

$$\ddot{q}_2 + 18.92 \dot{q}_2 + 358.11 q_2 = -37.63$$

$$\begin{Bmatrix} y_1 \\ y_2 \end{Bmatrix} = \begin{bmatrix} .073767 & .035002 \\ .042866 & -.090344 \end{bmatrix} \begin{Bmatrix} q_1 \\ q_2 \end{Bmatrix}.$$

From  $(q_0) = [A^*]^T [M] (y_0)$ , the modal-coordinate initial conditions are zero. From  $(\dot{q}_0) = [A^*]^T [M] (\dot{y}_0)$ , the modal-velocity initial conditions are

$$\begin{Bmatrix} \dot{q}_{10} \\ \dot{q}_{20} \end{Bmatrix} = \begin{bmatrix} .073767 & .042866 \\ .035002 & -.090344 \end{bmatrix} \begin{bmatrix} 150 & 0 \\ 0 & 100 \end{bmatrix} \begin{Bmatrix} 11.35 \\ 11.35 \end{Bmatrix}$$

$$= \begin{bmatrix} 11.065 & 4.2866 \\ 5.2503 & -9.0344 \end{bmatrix} \begin{Bmatrix} 11.35 \\ 11.35 \end{Bmatrix} = \begin{Bmatrix} 174.22 \\ -42.95 \end{Bmatrix}.$$

Substituting into,

$$q_1(t) = \frac{(A_{11}^* w_1 + A_{21}^* w_2)}{\omega_{n1}^2} + e^{-\zeta_1 \omega_{n1} t} (A_1 \cos \omega_{d1} t + B_1 \sin \omega_{d1} t)$$

$$q_2(t) = \frac{(A_{12}^* w_1 + A_{22}^* w_2)}{\omega_{n2}^2} + e^{-\zeta_2 \omega_{n2} t} (A_2 \cos \omega_{d2} t + B_2 \sin \omega_{d2} t) ,$$

nets

$$q_1(t) = \frac{149.5}{41.866} + e^{-0.3235t} (A_1 \cos 6.462 t + B_1 \sin 6.462 t)$$

$$q_2(t) = \frac{-37.63}{358.11} + e^{-0.946t} (A_2 \cos 18.90 t + B_2 \sin 18.90 t) ,$$

where

$$\omega_{d1} = \omega_{n1} \sqrt{1 - \zeta_1^2} = 6.470 \sqrt{1 - 0.0025} = 6.462$$

$$\omega_{d2} = \omega_{n2} \sqrt{1 - \zeta_2^2} = 18.92 \sqrt{1 - 0.0025} = 18.90 .$$

Imposing initial conditions for  $q_1(t)$

$$q_1(0) = 0 = \frac{149.5}{41.866} + A_1 \Rightarrow A_1 = -3.571$$

Further

$$\begin{aligned} \dot{q}_1(t) &= -0.3235 e^{-0.3235t} (A_1 \cos 6.462 t + B_1 \sin 6.462 t) \\ &\quad + 6.462 e^{-0.3235t} (-A_1 \sin 6.462 t + B_1 \cos 6.462 t) \end{aligned}$$

$$\therefore \dot{q}_1(0) = 174.22 = -0.3253 A_1 + 6.462 B_1$$

$$B_1 = \frac{174.22 + 0.3253 \times -3.571}{6.462} = 26.78$$

The complete solution satisfying the initial conditions is

$$q_1(t) = 3.571 + e^{-0.3235t} (-3.571 \cos 6.462 t + 26.78 \sin 6.462 t)$$

Similarly, the complete solution for  $q_2(t)$  is

$$q_2(t) = -0.1051 + e^{-0.946t} (0.1051 \cos 18.90 t + B_2 \sin 18.90 t)$$

$$\begin{aligned} \dot{q}_2(t) &= -0.946 e^{-0.946t} (0.1051 \cos 18.90 t + B_2 \sin 18.90 t) \\ &\quad + e^{-0.946t} 18.90 (0.1051 \sin 18.90 t - B_2 \cos 18.90 t) \end{aligned}$$

$$\therefore \dot{q}_2(0) = -42.95 = -0.946 \times 0.1051 - 18.90 B_2 \Rightarrow B_2 = 2.267$$

The complete solution for  $q_2(t)$  satisfying the initial conditions is

$$q_2(t) = -0.1051 + e^{-0.946t}(0.1051 \cos 18.90t + 2.267 \sin 18.90t)$$

The physical solution is

$$\begin{Bmatrix} y_1 \\ y_2 \end{Bmatrix} = q_1(t) \begin{Bmatrix} .073767 \\ .042866 \end{Bmatrix} + q_2(t) \begin{Bmatrix} 0.035002 \\ -0.090344 \end{Bmatrix}.$$