Lecture 2

Read textbook CHAPTER 1.4, Apps B&D

Today: Derive EOMs & Linearization

Fundamental equation of motion for mass-spring-damper system (1DOF). Linear and nonlinear system. Examples of derivation of EOMs

Appendix A Equivalence of principles of conservation of mechanical energy and conservation of linear momentum.

Appendix B: Linearization

Work problems:

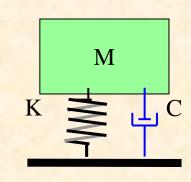
Chapter 1: 5, 8, 13, 14, 15, 20, 43, 44, 56

Lecture 2 ME617

Kinetics of 1-DOF mechanical systems

The fundamental elements in a mechanical system and the process to set a coordinate system and derive an equation of motion.

LINEARIZATION included.

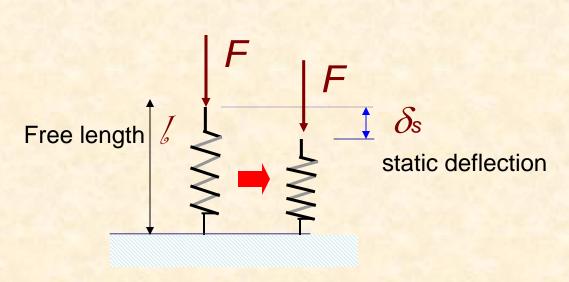


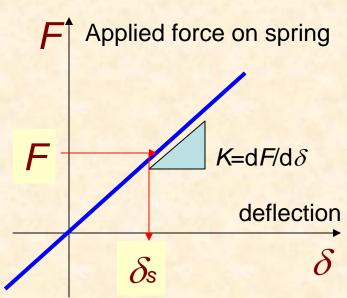
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A system with an elastic element (linear spring)

Linear elastic element (spring-like)





Notes:

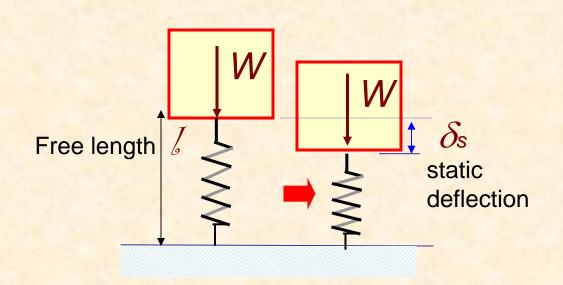
- a) Spring element is regarded as massless
- b) Applied force is STATIC
- c) Spring reacts with a force proportional to deflection, $Fs = -K\delta_s$, and stores potential energy
- d) K = stiffness coefficient [N/m or lbf/in] is constant

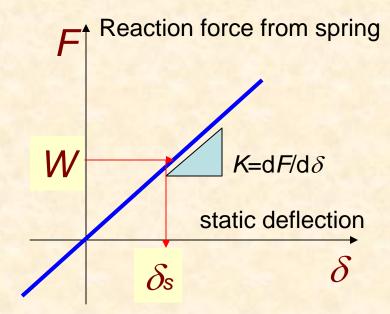
Balance of static forces

$$F_s = -K \delta_s$$
 F_s

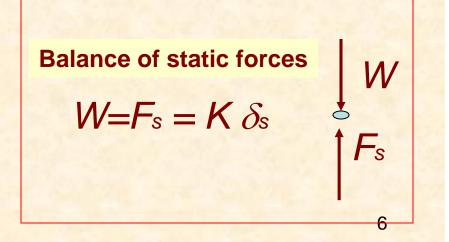
Statics of system with elastic & mass elements

Linear spring + added weight





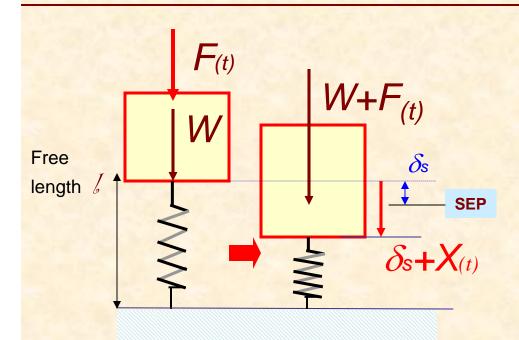
- a) Block has weight **W= Mg**
- b) Block is regarded as a point mass

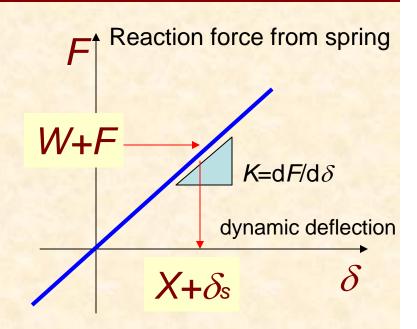


Dynamics of system with elastic & mass elements

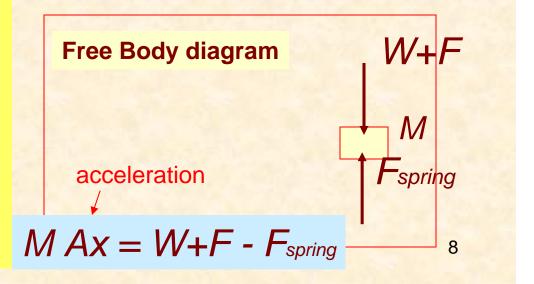
Derive the equation of motion (EOM) for the system

Linear spring + weight (mass x g) + force $F_{(t)}$

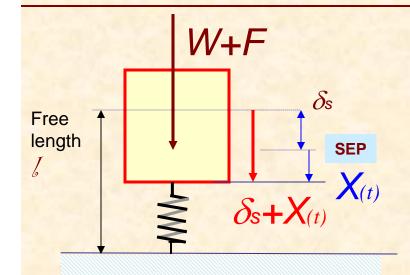




- a) Coordinate X describing motion has origin at Static Equilibrium Position (SEP)
- b) For free body diagram, assume state of motion, for example $X_{(t)}>0$
- c) Then, state Newton's equation of motion
- d) Assume no lateral (side motions)



Derive the equation of motion



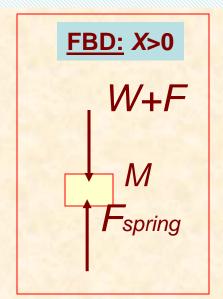
$$MAx = W+F - F_{spring}$$



$$F_{spring} = K(X + \delta_s)$$

$$M Ax = W+F - K(X+\delta_s)$$

$$M Ax = (W-K\delta_s) + F - KX$$



Cancel terms from force balance at SEP to get

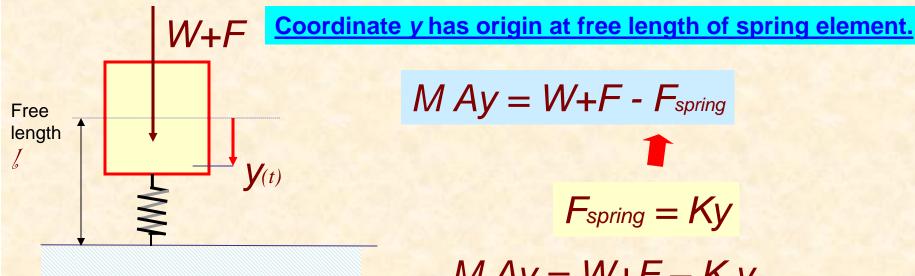
$$MAx = +F - KX$$

$$MAx + KX = F_{(t)}$$

$$A_X = \frac{d^2 X}{d t^2} = \ddot{X}$$

Note: Motions from **SEP**

Another choice of coordinate system



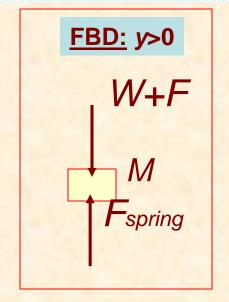
 $MAy = W+F - F_{spring}$



$$F_{spring} = Ky$$

$$MAy = W+F-Ky$$

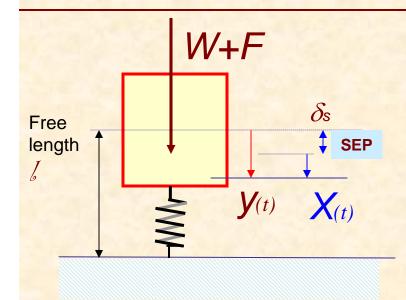
Weight (static force) remains in equation



$$Ay + Ky = W + F_{(t)}$$

$$A_y = \frac{d^2 y}{dt^2} = \ddot{y}$$

EOM in two coordinate systems



$$y = X + \delta_s$$
 $\ddot{y} = \ddot{X}$

$$F_{spring} = Ky = K(X + \delta_s)$$

Coordinate y has origin at free length of spring element. X has origin at SEP.

$$MAy + Ky = W + F_{(t)}$$
 (1)

$$A_{y} = \frac{d^{2} y}{d t^{2}} = \ddot{y}$$

$$MAx + KX = F_{(t)}$$
 (2)

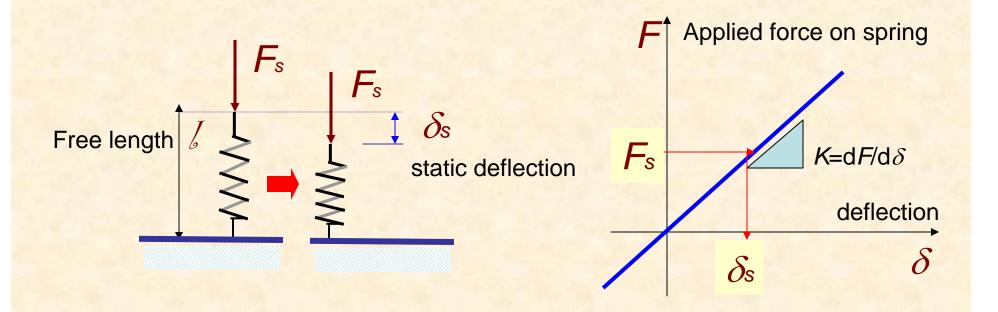
$$A_X = \frac{d^2 X}{d t^2} = \ddot{X}$$

- (?) Are Eqs. (1) and (2) the same?
- (?) Do Eqs. (1) and (2) represent the same system?
- (?) Does the weight disappear?
- (?) Can I just cancel the weight?

K-M system with dissipative element (a viscous dashpot)

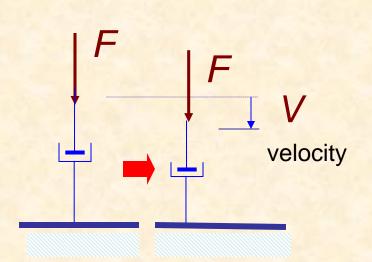
Derive the equation of motion (EOM) for the system

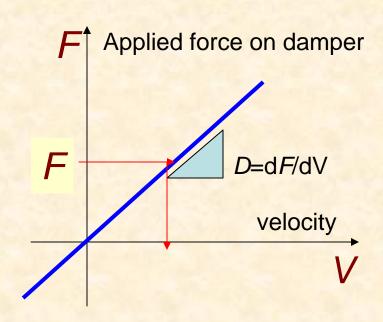
Recall: a linear elastic element



- a) Spring element is regarded as massless
- b) K = stiffness coefficient is constant
- c) Spring reacts with a force proportional to deflection and stores potential energy

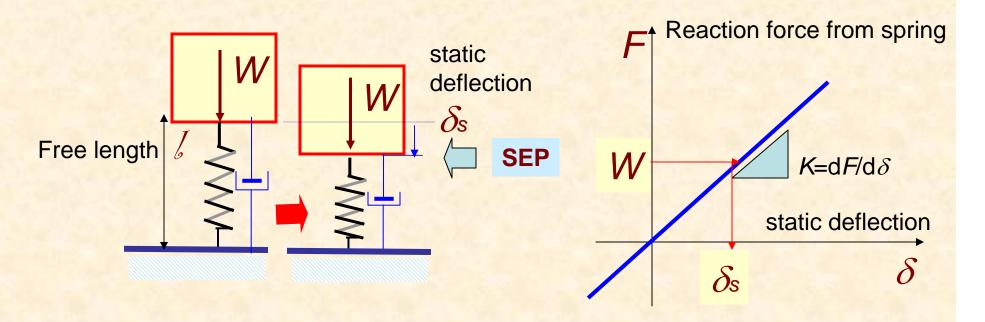
(Linear) viscous damper element





- a) Dashpot element (damper) is regarded as massless
- b) D =damping coefficient [N/(m/s) or lbf/(in/s)] is constant
- A damper needs velocity to work; otherwise it <u>can not</u> dissipate mechanical energy
- d) Under static conditions (no motion), a damper does NOT react with a force

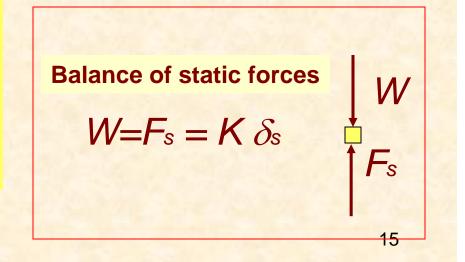
Spring + Damper + Added weight



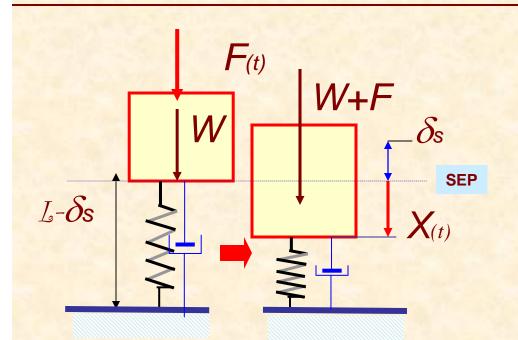
Notes:

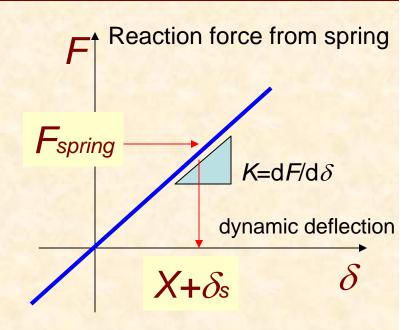
- a) Block has weight W=Mg and is regarded as a point mass.
- b) Weight applied very slowly static condition.
- c) Damper **does NOT react** to a static action, i.e. $F_D = 0$

SEP: static equilibrium position

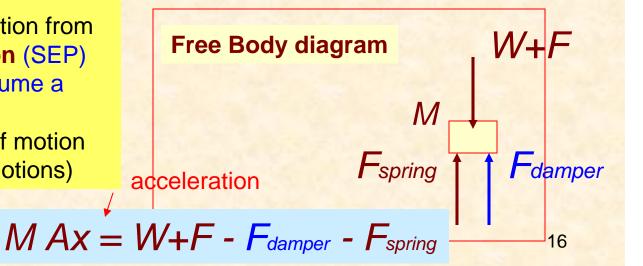


Spring + Damper + Weight + force $F_{(t)}$

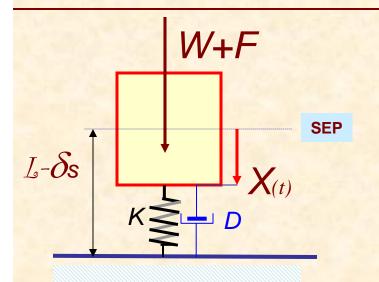


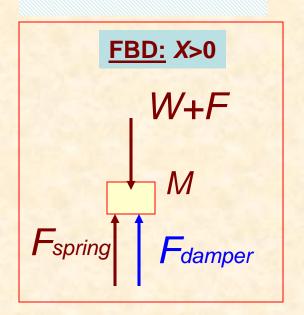


- a) Coordinate X describes motion from Static Equilibrium Position (SEP)
- b) For free body diagram, assume a state of motion $X_{(t)}>0$
- c) State Newton's equation of motion
- d) Assumed no lateral (side motions)



Equation of motion: spring-damper-mass





 $MAx = W+F_{(t)} - F_{damper} - F_{spring}$

$$A_X = \frac{d^2 X}{d t^2} = \ddot{X}$$
 Fedamper = D V_X

$$F_{damper} = D V_{x}$$

$$V_X = \frac{dX}{dt} = \dot{X}$$

$$V_X = \frac{dX}{dt} = \dot{X}$$
 $F_{\text{spring}} = K(X + \delta_{\text{s}})$

$$MAx = W+F - K(X+\delta_s) - DV_x$$

$$MAx = (W-K\delta_s) + F - KX - DV_X$$

Cancel terms from force balance at SEP to get

$$MAx = +F - KX - DV_X$$

$$MAX + DV_X + KX = F_{(t)}$$

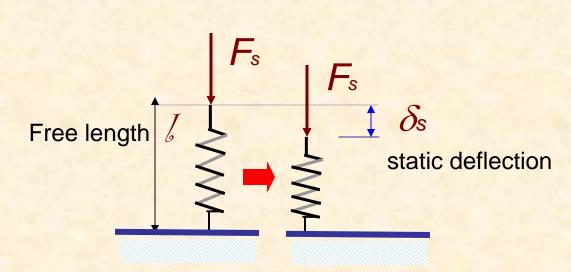


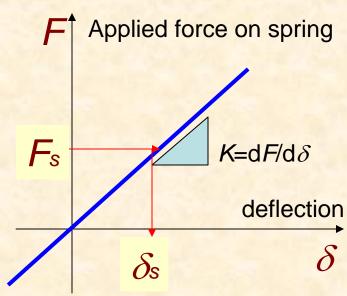
EOM:
$$M \ddot{X} + D \dot{X} + K X = F_{(t)}$$

Simple nonlinear mechanical system

Derive the equation of motion (EOM) for the system and linearize EOM about SEP

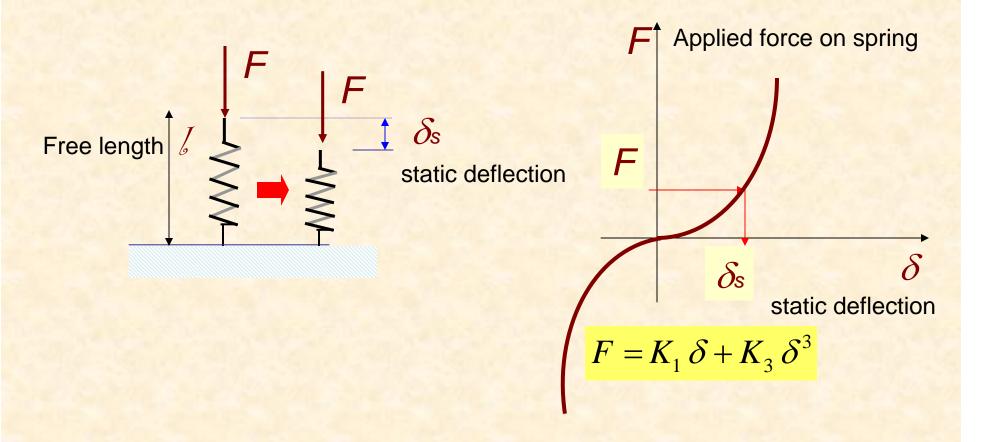
Recall a linear spring element





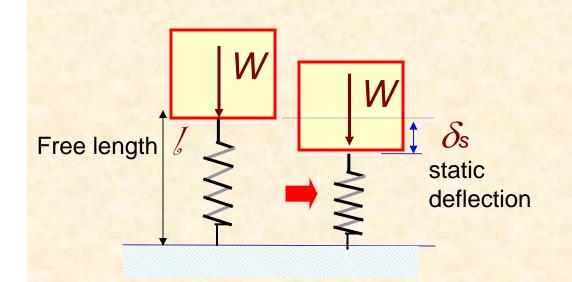
- a) Spring element is regarded as massless
- b) K = stiffness coefficient is constant
- c) Spring reacts with a <u>force proportional to</u> <u>deflection</u> and stores potential energy

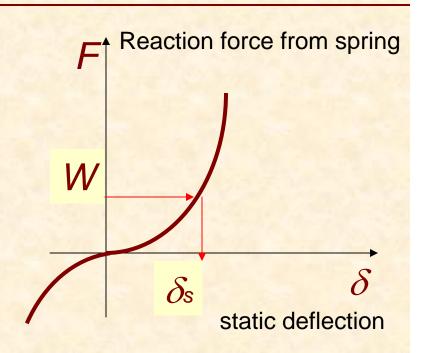
A nonlinear spring element



- a) Spring element is massless
- b) Force vs. deflection curve is **NON linear**
- c) K₁ and K₃ are material parameters [N/m, N/m³]

Linear spring + added weight



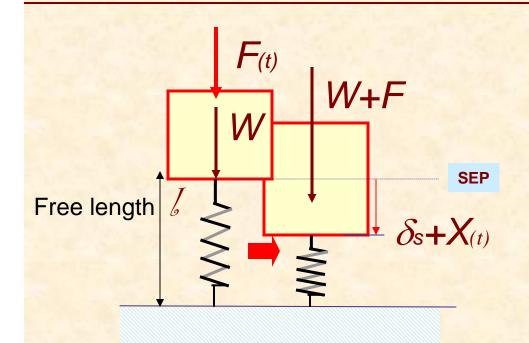


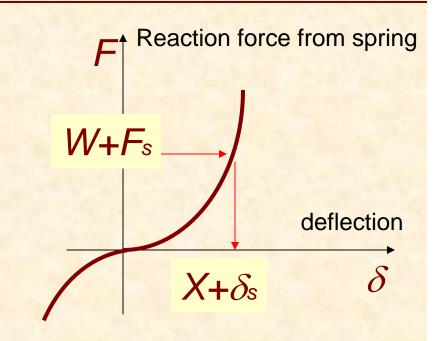
Notes:

- a) Block has weight *W*= *Mg*
- Block is regarded as a point mass
- c) Static deflection δ s found from

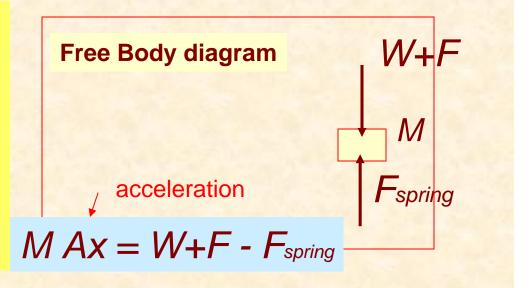
Balance of static forces solving nonlinear equation: $W = F_{spring} = K_1 \, \delta_s + K_3 \, \delta_s^3$ **F**spring

Nonlinear spring + weight + force $F_{(t)}$

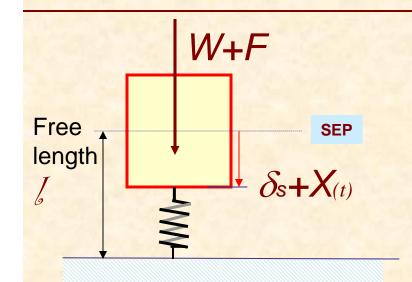




- a) Coordinate X describing motion has origin at Static Equilibrium Position (SEP)
- b) For free body diagram, assume state of motion, for example $X_{(t)}>0$
- c) Then, state Newton's equation of motion
- d) Assume no lateral (side motions)



Nonlinear Equation of motion



$$M \ddot{X} = F_{(t)} + W - F_{spring}$$

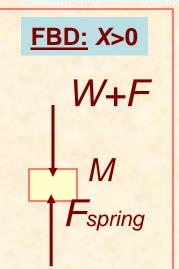
$$A_X = \frac{d^2 X}{d t^2} = \ddot{X}$$



$$F_{spring} = K_1 \left(\delta_s + X \right) + K_3 \left(\delta_s + X \right)^3$$

$$M \ddot{X} = F_{(t)} + W - K_1 (\delta_s + X) - K_3 (\delta_s + X)^3$$

Expand RHS:



$$M \ddot{X} = F_{(t)} + W - K_1 (\delta_s + X) - K_3 (\delta_s^3 + 3\delta_s^2 X + 3\delta_s X^2 + X^3)$$

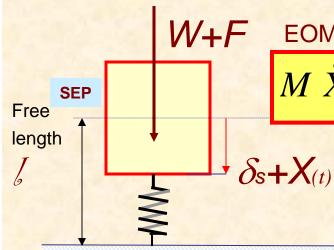
$$M \ddot{X} = F_{(t)} + \left(W - K_1 \delta_s - K_3 \delta_s^3\right) - \left(K_1 + 3K_3 \delta_s^2\right) X - K_3 \left(3\delta_s X^2 + X^3\right)$$

Cancel terms from force balance at SEP to get

$$M \ddot{X} + (K_1 + 3K_3\delta_s^2)X + K_3(3\delta_s X^2 + X^3) = F_{(t)}$$

Notes: Motions are from SEP

Linearize equation of motion



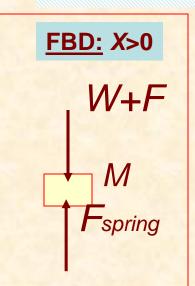
EOM is nonlinear:

$$M \ddot{X} + (K_1 + 3K_3\delta_s^2)X + K_3(3\delta_s X^2 + X^3) = F_{(t)}$$

Assume motions $X(t) \ll \delta s$

which means $|F(t)| \ll W$

and set $X^2 \sim 0$, $X^3 \sim 0$



to obtain the linear EOM:

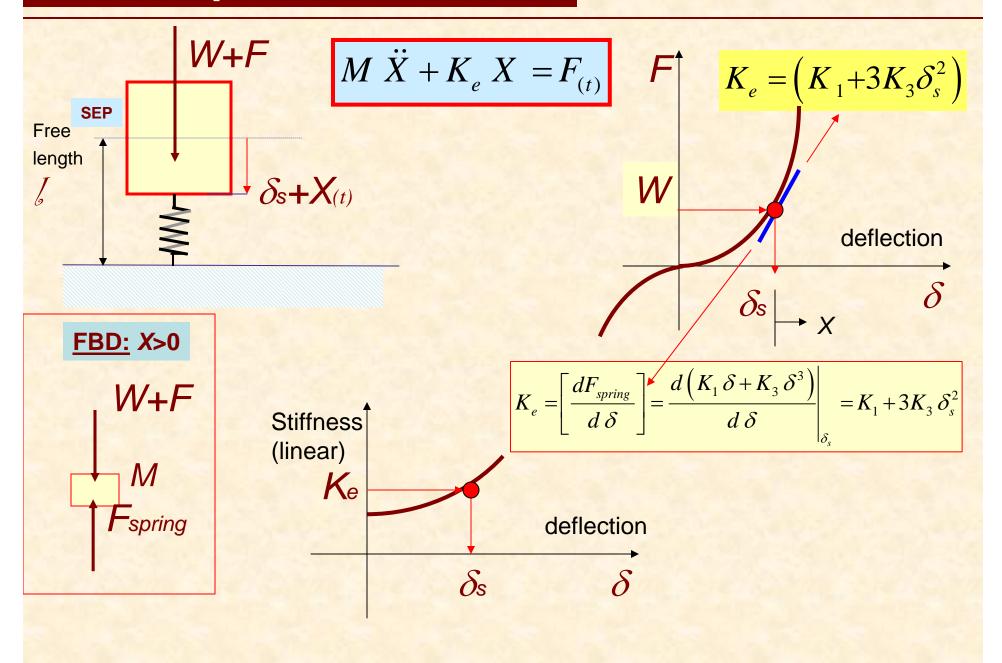
$$M \ddot{X} + K_e X = F_{(t)}$$

where the linearized stiffness
$$K_e = (K_1 + 3K_3\delta_s^2)$$

is a function of the static condition

$$K_e = \left[\frac{dF_{spring}}{d\delta}\right] = \frac{d\left(K_1 \delta + K_3 \delta^3\right)}{d\delta}\bigg|_{\delta_s} = K_1 + 3K_3 \delta_s^2$$

Linear equation of motion



Read & rework

Examples of derivation of EOMS for physical systems available on class URL site(s)

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