

Lecture 29. GENERAL MOTION/ROLLING-WITHOUT-SLIPPING EXAMPLES

General equations of Motion

Force Equation

$$\sum f_{iX} = m \ddot{\mathbf{R}}_{gX}, \quad \sum f_{iY} = m \ddot{\mathbf{R}}_{gY}. \quad (5.15)$$

General Moment Equation

$$\sum M_{oz} = I_o \ddot{\theta} + m(\mathbf{b}_{og} \times \ddot{\mathbf{R}}_o)_z. \quad (5.24)$$

Moments About the Mass Center

$$M_{gz} = I_g \ddot{\theta}. \quad (5.25)$$

Moments About a Fixed axis

$$M_{oz} = I_o \ddot{\theta}. \quad (5.26)$$

The examples of this lecture will be analyzed using $\Sigma \mathbf{f} = m \ddot{\mathbf{R}}_g$ and $\Sigma M_{gz} = I_g \ddot{\theta}$.

Kinetic Energy of a Rigid Body

$$T = \frac{m |\dot{\mathbf{R}}_g|^2}{2} + \frac{I_g \dot{\theta}^2}{2}, \quad (5.205)$$

A Cylinder Rolling Down An Inclined Plane

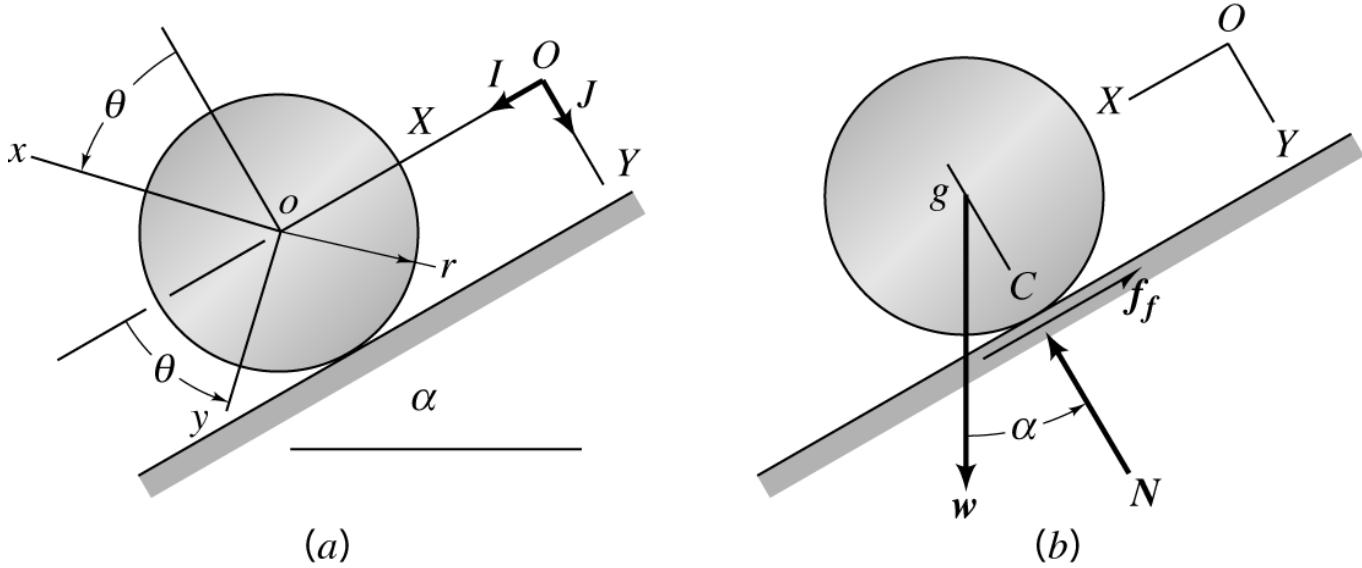


Figure 5.25 (a) Uniform disk of radius r and mass m rolling (without slipping) down an inclined plane, (b) Free-body diagram. The static Coulomb coefficient of friction for the plane is μ_s .

Derive the governing differential equation of motion for rolling without slipping.

Force Equation Components

$$\sum f_X = w \sin \alpha - f_f = m \ddot{X} \quad (5.75)$$

$$\sum f_Y = w \cos \alpha - N = m \ddot{Y} = 0 \Rightarrow N = W \cos \alpha.$$

Moment Equation

$$\Sigma M_{\theta g} = f_f r = I_g \ddot{\theta} = \frac{mr^2}{2} \ddot{\theta}. \quad (5.76)$$

Eq.(5.76) and the first of Eq.(5.75) constitute two equations in the three unknowns: $\ddot{\theta}$, \ddot{X} , and f_f .

Rolling-without-slipping kinematic constraint

$$\ddot{X} = r \ddot{\theta} . \quad (5.77)$$

Solving for f_f from Eq.(5.76), and substituting into the first of Eq.(5.75) gives

$$m \ddot{X} = w \sin \alpha - m \frac{r}{2} \ddot{\theta}.$$

Now, substituting for $\ddot{\theta} = \ddot{X}/r$ from Eq.(5.77) gives

$$m \ddot{X} + m \frac{r}{2} \cdot \frac{\ddot{X}}{r} = \frac{3m}{2} \ddot{X} = w \sin \alpha \Rightarrow \ddot{X} = \frac{2g}{3} \sin \alpha. \quad (5.78)$$

Using θ as the dependent variable, solve the first of Eq.(5.75) for f_f and then substitute into Eq.(5.76) to obtain

$$I_g \ddot{\theta} = r(w \sin \alpha - m \ddot{X}) ,$$

Substituting $\ddot{X} = r \ddot{\theta}$ from Eq.(5.77) gives

$$(I_g + mr^2)\ddot{\theta} = \frac{3mr^2}{2}\ddot{\theta} = wr\sin\alpha. \quad (5.79)$$

Comparisons of Eqs.(5.78) and (5.79) show basically the same equation.

Friction Force

$$\text{From, } rf_f = m \frac{r^2}{2} \ddot{\theta}, \quad f_f = 0 \Rightarrow \ddot{\theta} = 0$$

$$\text{From, } w\sin\alpha - f_f = m\ddot{X}, \quad f_f = 0 \Rightarrow \ddot{X} = g\sin\alpha.$$

The friction force causes the cylinder to rotate and reduces the acceleration to $\ddot{X} = (2/3)g\sin\alpha$.

How much Coulomb friction is required to prevent slipping?

$$f_f = w\sin\alpha - m\ddot{X} = w\sin\alpha - m\left(\frac{2g}{3}\sin\alpha\right) = \frac{w}{3}\sin\alpha. \quad (5.80)$$

Since, $N = w\cos\alpha$, the “required” static Coulomb friction force coefficient to prevent slipping is

$$\mu_s(\text{required}) = \frac{f_f}{N} = \frac{w\sin\alpha}{3} \times \frac{1}{w\cos\alpha} = \frac{\tan\alpha}{3}. \quad (5.81)$$

If this calculated value is less than or equal to μ_s , the wheel will roll without slipping. If it greater than μ_s , the wheel will slip, and $f_f = \mu_d N$.

Slipping Motion Equations of Motion. For slipping $f_f = \mu_d N = \mu_d w \cos \alpha$, the cylinder has two degrees of freedom, and the equations of motion are

$$w \sin \alpha - \mu_d w \cos \alpha = m \ddot{X}$$

$$\frac{mr^2}{2} \ddot{\theta} = r \mu_d w \cos \alpha .$$

Deriving the equation of Motion for Rolling-Without-Slipping from Conservation of Energy

Without slipping, energy is conserved and $T + V = T_0 + V_0$. Taking the origin of the X, Y system as the datum for potential energy,

$$V_g = -w X \sin \alpha . \quad (\text{i})$$

The kinetic energy is defined to be

$$T = \frac{m}{2} \dot{X}^2 + \frac{mr^2}{4} \dot{\theta}^2 = \frac{m}{2} \dot{X}^2 + \frac{mr^2}{4} \left(\frac{\dot{X}}{r} \right)^2 = \frac{3m}{4} \dot{X}^2 , \quad (\text{ii})$$

where the rolling without slipping relationship $\dot{X} = r\dot{\theta}$ has been used. Substituting from (i) and (ii) gives

$$\frac{3m}{2}\left(\frac{\dot{X}^2}{2}\right) - wX \sin \alpha = T_0 + V_0 .$$

Differentiating w.r.t. X

$$\frac{3m}{2} \frac{d}{dX}\left(\frac{\dot{X}^2}{2}\right) - w \sin \alpha = 0 \Rightarrow \frac{3m}{2} \ddot{X} = w \sin \alpha .$$

An Imbalanced Cylinder Rolling Down an Inclined Plane

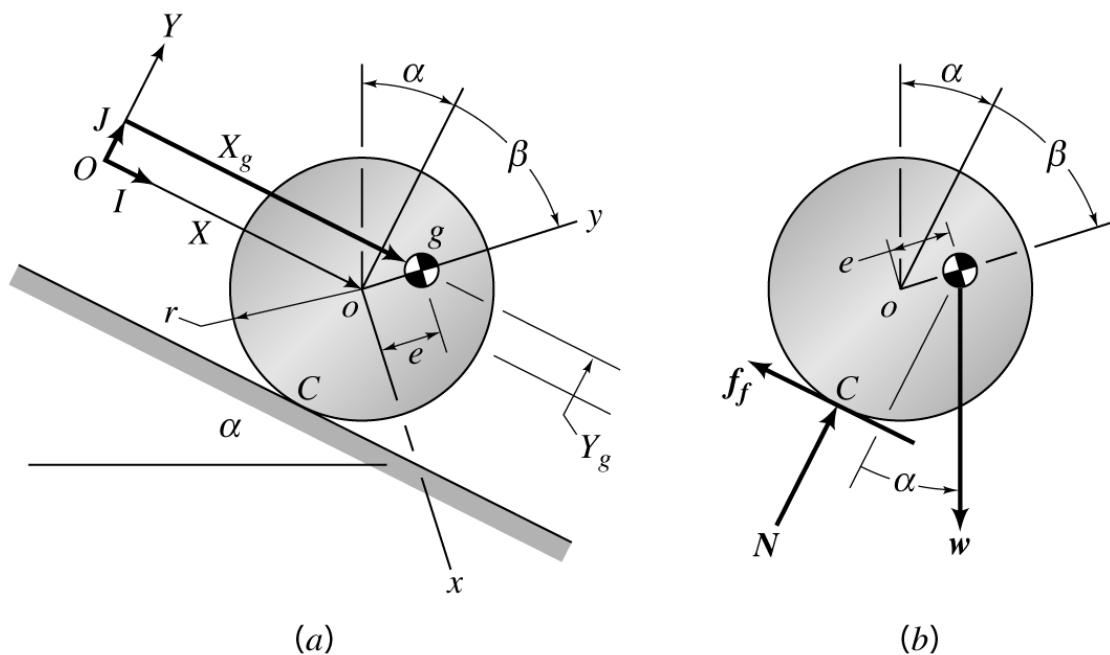


Figure 5.26 (a) Disk with its mass center displaced a distance e from its geometrical center, rolling down an inclined plane, (b) Free-body diagram.

The disk's mass center is located in the X , Y system by:

$$X_g = X + e \sin \beta , \quad Y_g = e \cos \beta . \quad (5.83)$$

The rolling-without-slipping kinematic condition for figure 5.26A is

$$\ddot{X} = r \ddot{\beta} . \quad (5.84)$$

Without slipping, the disk has two variables, X and β , but only one degree of freedom. The radius of gyration of the disk about point o is k_{og} ; hence, $I_o = m k_{og}^2$.

Derive the governing differential equation of motion.

Solution A. Take moments about the mass center.

Applying $\Sigma f = m \ddot{\vec{R}}_g$ for the disk's mass center gives:

$$\begin{aligned} \Sigma f_X &= w \sin \alpha - f_f = m \ddot{X}_g \\ \Sigma f_Y &= N - w \cos \alpha = m \ddot{Y}_g . \end{aligned} \quad (5.85)$$

In reviewing these equations, note that $\ddot{Y}_g \neq 0$.

Taking moments about the mass center, the moment equation is

$$\Sigma M_g = N e \sin \beta + f_f(r + e \cos \beta) = I_g \ddot{\beta} . \quad (5.86)$$

Note that positive moments are in the $+ \beta$, clockwise direction. Also, from the parallel-axis formula, $I_g = I_o - m e^2 = m(k_g^2 - e^2)$.

Eqs.(5.84), (5.85) and (5.86) provide four equations in the six unknowns: \ddot{X} , $\ddot{\beta}$, \ddot{X}_g , \ddot{Y}_g , N , and f_f .

Kinematics. Differentiating Eqs.(5.83) once with respect to time gives

$$\dot{X}_g = \dot{X} + e \cos \beta \dot{\beta} , \quad \dot{Y}_g = -e \sin \beta \dot{\beta} .$$

Differentiating a second time and substituting for $\ddot{X} = r \ddot{\beta}$ gives

$$\ddot{X}_g = r \ddot{\beta} + e \cos \beta \ddot{\beta} - e \sin \beta \dot{\beta}^2 , \quad \ddot{Y}_g = -e \sin \beta \ddot{\beta} - e \cos \beta \dot{\beta}^2 , \quad (5.87)$$

which provides our final two equations.

The governing equation of motion is obtained by the following steps:

a. Substitute for \ddot{X}_g, \ddot{Y}_g from Eq.(5.87) into Eqs (5.85), obtaining

$$f_f = w \sin \alpha - m(r \ddot{\beta} + e \cos \beta \ddot{\beta} - e \sin \beta \dot{\beta}^2) \quad (5.88)$$

$$N = w \cos \alpha - m(e \sin \beta \ddot{\beta} + e \cos \beta \dot{\beta}^2).$$

b. Substitute for N and f_f into Eq.(5.86), obtaining

$$I_g \ddot{\beta} = [w \cos \alpha - m(e \sin \beta \ddot{\beta} + e \cos \beta \dot{\beta}^2)]e \sin \beta + [w \sin \alpha - m(r \ddot{\beta} + e \cos \beta \ddot{\beta} - e \sin \beta \dot{\beta}^2)](r + e \cos \beta).$$

After a fair amount of algebra, the governing equation is

$$m(k_{og}^2 + r^2 + 2r \cos \beta) \ddot{\beta} - m e \sin \beta \dot{\beta}^2 = w[r \sin \alpha + e \sin(\beta + \alpha)]. \quad (5.89)$$

Note: $I_o = m k_{og}^2 \Rightarrow I_g = I_o - m e^2 = m(k_{og}^2 - e^2)$.

This equation reduces to Eq.(5.79) if $e = 0$, and $I_o = m r^2 / 2$.

The energy-integral substitution, $\ddot{\beta} = d(\dot{\beta}^2 / 2) / d\beta$, converts Eq.(5.89) to

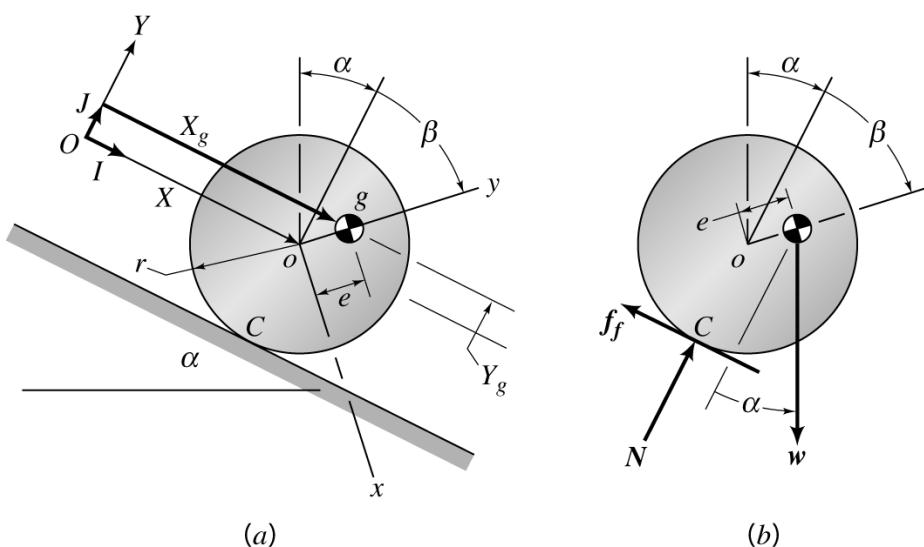
$$\frac{d}{d\beta} [m(k_{og}^2 + r^2 + 2r \cos \beta) (\frac{\dot{\beta}^2}{2})] = w[r \sin \alpha + e \sin(\beta + \alpha)].$$

For the boundary conditions ($\beta(0) = 0$; $\dot{\beta}(0) = 0$); integration gives

$$m(k_{og}^2 + r^2 + 2re\cos\beta)\left(\frac{\dot{\beta}^2}{2}\right) = w[r\sin\alpha\beta - e\cos(\beta + \alpha) + e\cos\alpha] . \quad (5.90)$$

Without slipping, there is no energy dissipation.

Solution B: Take moments about C.



For moments about C , the EOM is

$$\sum \mathbf{M}_C = I_C \ddot{\beta} - m(\mathbf{b}_{Cg} \times \ddot{\mathbf{R}}_C) ,$$

where clockwise moments are positive (positive β rotation).

Kinematics:

$$\mathbf{b}_{Cg} = \mathbf{I}e \sin \beta + \mathbf{J}(r + e \cos \beta) , \quad \ddot{\mathbf{R}}_c = \mathbf{J}r \dot{\beta}^2$$

$$\therefore \mathbf{b}_{Cg} \times \ddot{\mathbf{R}}_c = K e r \dot{\beta}^2 \sin \beta$$

Inertia properties:

$$I_g = I_o - m e^2 = m k_{og}^2 - m e^2$$

$$\begin{aligned} I_C &= I_g + m |b_{gC}|^2 = (m k_{og}^2 - m e^2) + m [(r + e \cos \beta)^2 + (e \sin \beta)^2] \\ &= m k_{og}^2 + m(r^2 + 2re \cos \beta) \end{aligned}$$

External moment about C due to weight

$$\begin{aligned} \mathbf{M}_C &= -(r_{Cg} \times w) \\ &= -[\mathbf{I}e \sin \beta + \mathbf{J}(r + e \cos \beta)] \times w(\mathbf{I} \sin \alpha + \mathbf{J} \cos \alpha) \\ &= \mathbf{K}(w e \sin \beta \cos \alpha + r w \sin \alpha + w e \sin \alpha \cos \beta) \\ &= \mathbf{K}[w r \sin \alpha + w e \sin(\alpha + \beta)] \end{aligned}$$

Plugging in the results gives (again)

$$\begin{aligned} m(k_{og}^2 + r^2 + 2r e \cos \beta) \ddot{\beta} - m e r \sin \beta \dot{\beta}^2 \\ = w[r \sin \alpha + e \sin(\beta + \alpha)]. \end{aligned} \tag{5.89}$$

This approach is obviously quicker.

Deriving the equation of Motion from Conservation of Energy

Applying $T + V = T_0 + V_0$, and using the origin of the X, Y system for the gravity potential-energy function gives

$$\begin{aligned} \frac{I_g}{2} \dot{\beta}^2 + \frac{m}{2} (\dot{X}_g^2 + \dot{Y}_g^2) - w X \sin \alpha + w e \cos(\alpha + \beta) \\ = (T_0 + V_0) . \end{aligned} \quad (5.223)$$

This example has three coordinates X_g, Y_g, β . To eliminate unwanted coordinates, we need the rolling-without-slipping condition $X = r\beta$, plus the kinematic conditions,

$$\begin{aligned} X_g &= X + e \sin \beta = r\beta + e \sin \beta \Rightarrow \dot{X}_g = r\dot{\beta} + e \cos \beta \dot{\beta} \\ Y_g &= e \cos \beta \Rightarrow \dot{Y}_g = -e \sin \beta \dot{\beta} . \end{aligned}$$

Substituting into Eq.(5.223) gives

$$\begin{aligned} m(k_{og}^2 + r^2 + 2er \cos \beta) \frac{\dot{\beta}^2}{2} \\ - w[r\beta \sin \alpha - e \cos(\alpha + \beta)] = (T_0 + V_0) , \end{aligned} \quad (5.224)$$

Differentiating with respect to β gives the DEQ. of motion

$$\begin{aligned}
& m(k_{og}^2 + r^2 + 2er\cos\beta)\ddot{\beta} - mer\sin\beta\dot{\beta}^2 \\
& = w[r\sin\alpha + e\sin(\alpha + \beta)] . \quad (5.204)
\end{aligned}$$