

FREQUENCY RESPONSE FUNCTIONS FOR SDOF systems

Dimension	Displacement / Force	Velocity / Force	Acceleration / Force
Name	Admittance, Compliance, Receptance	Mobility	Accelerance, Inertance

Dimension	Force / Displacement	Force / Velocity	Force / Acceleration
Name	Dynamic Stiffness	Mechanical Impedance	Apparent Mass, Dynamic Mass

$$M \cdot \frac{d^2}{dt^2} X + D \cdot \frac{d}{dt} X + K \cdot X = F_0 \cdot e^{i \cdot \omega \cdot t} \quad \text{EOM for periodic load}$$

$$i = \sqrt{-1}$$

Let $X(t) = Z \cdot e^{i \cdot \omega \cdot t}$ and substitute into EOM to obtain
 Z E complex #

$$\left[(K - M \cdot \omega^2) + i \cdot \omega \cdot D \right] \cdot (Z \cdot e^{i \cdot \omega \cdot t}) = F_0 \cdot e^{i \cdot \omega \cdot t}$$

Hence,

$$\frac{Z}{F_0} = \frac{1}{\left[(K - M \cdot \omega^2) + i \cdot \omega \cdot D \right]} \quad \text{OUTPUT/INPUT is the Transfer function}$$

Define

$$M := 10 \cdot \text{kg}$$

$$K_{\text{www}} := 3.948 \cdot 10^6 \cdot \frac{\text{N}}{\text{m}}$$

$$\omega_n := \left(\frac{K}{M} \right)^{.5} = 628.331 \frac{\text{rad}}{\text{s}} \quad \text{natural frequency}$$

$$f_n := \frac{\omega_n}{2 \cdot \pi} = 100.002 \text{ Hz}$$

Set damping ratios:

$$\zeta_1 := 0.05$$

$$\zeta_2 := 2 \cdot \zeta_1$$

$$\zeta_3 := 4 \cdot \zeta_1$$

$$D_1 := \zeta_1 \cdot 2 \cdot \sqrt{K \cdot M} = 628.331 \text{ N} \cdot \frac{\text{s}}{\text{m}}$$

Since Z E C, then $Z = X_A \cdot e^{-i \cdot \varphi}$: amplitude and phase φ

Thus

$$X(t) = X_A \cdot e^{i \cdot (\omega \cdot t - \varphi)}$$

where

$$\frac{X_A}{F_o} = \frac{1}{\sqrt{[(K - M \cdot \omega^2)^2 + (\omega \cdot D)^2]}}$$

and

$$\tan(\varphi) = \frac{\omega \cdot D}{K - M \cdot \omega^2}$$

Introduce parameters

NATURAL frequency:

$$\omega_n = \sqrt{\frac{K}{M}}$$

DAMPING ratio

$$\zeta = \frac{D}{2 \cdot \sqrt{K \cdot M}}$$

Operating frequency ratio: $r = \frac{\omega}{\omega_n}$

The transfer function **DISPLACEMENT/FORCE** equals

COMPLIANCE, ADMITTANCE or FLEXIBILITY FN.

$$\frac{X_A}{F_o} = \frac{1}{\sqrt{[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2]}} \cdot \frac{1}{K}$$

$$\tan(\varphi) = \frac{2 \cdot \zeta \cdot r}{1 - r^2}$$

displacement/force
units of 1/stiffness

DYNAMIC STIFFNESS FN : input/output.

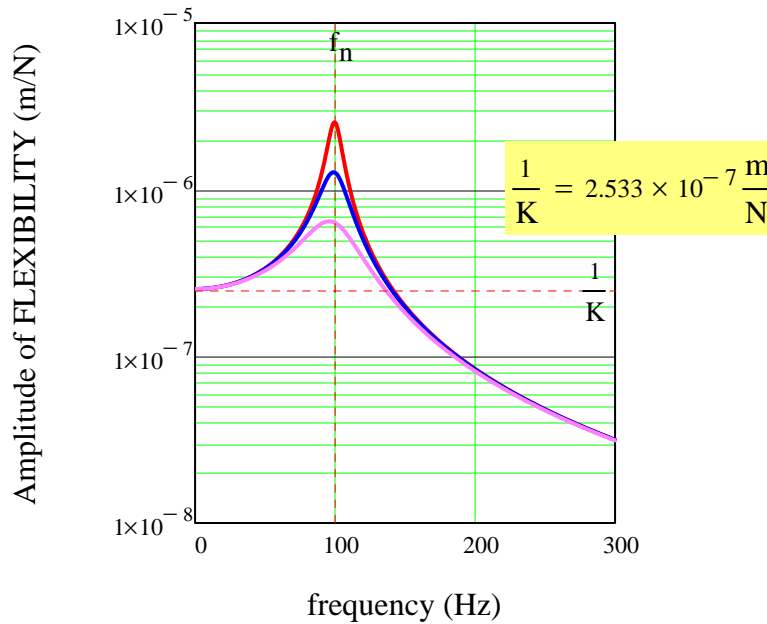
$$\frac{F_o}{X_A} = K \cdot \sqrt{[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2]}$$

Flexibility function

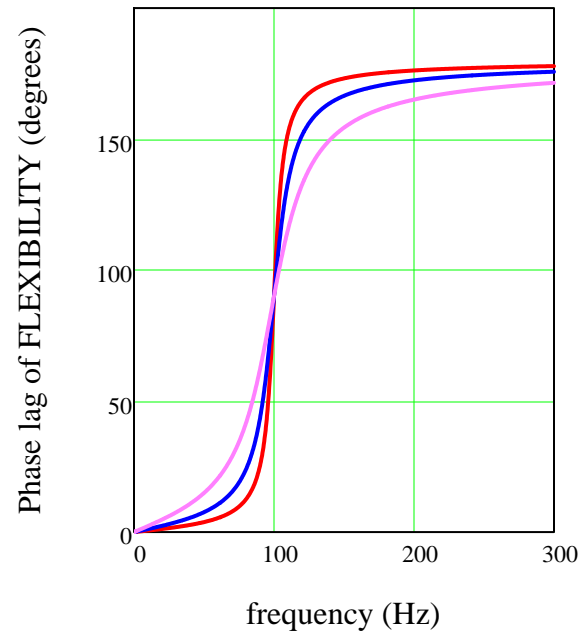
$$\frac{X_A}{F_0}$$

$$\text{Flex}(r, \zeta) := \frac{K^{-1}}{\sqrt{\left[(1-r^2)^2 + (2\zeta \cdot r)^2 \right]}}$$

$$\varphi(r, \zeta) := \begin{cases} \varphi \leftarrow \text{atan} \left(\frac{2 \cdot \zeta \cdot r}{1 - r^2} \right) \cdot \left(\frac{180}{\pi} \right) \\ \varphi \leftarrow \varphi + 180 \text{ if } r > 1 \\ \varphi \end{cases}$$



- Xsi1=0.05
- Xsi2=2 x Xsi1
- Xsi3=2 x Xsi2



- Xsi1=0.05
- Xsi2=2 x Xsi1
- Xsi3=2 x Xsi2

At times the **velocity** is measured rather than the displacement, hence from

$$X(t) = Z \cdot e^{i \cdot \omega \cdot t}$$

obtain
$$V_X(t) = Z \cdot i \cdot \omega \cdot e^{i \cdot \omega \cdot t} = \omega \cdot Z \cdot e^{i \left(\omega \cdot t + \frac{\pi}{2} \right)}$$

$$V_X(t) = \omega \cdot X_A \cdot e^{i \left(\omega \cdot t + \frac{\pi}{2} - \varphi \right)} = v_A \cdot e^{i \left(\omega \cdot t - \varphi_V \right)}$$

and the **amplitude of the transfer function (velocity/force)** is

$$\frac{v_A}{F_O} = \frac{\omega}{\sqrt{\left[(K - M \cdot \omega^2)^2 + (\omega \cdot D)^2 \right]}} \quad \text{and} \quad \varphi_V = \varphi - \frac{\pi}{2}$$

Using the nat. frequency and damping ratio (ω_n, ζ) gives

MOBILITY fn.

$$\frac{v_A}{F_O} = \frac{1}{\sqrt{\left[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2 \right]}} \cdot \frac{\omega}{K}$$

velocity/force units of 1/Damping

While the

MECHANICAL IMPEDANCE

$$\frac{F_O}{v_A} = \frac{K}{\omega} \cdot \sqrt{\left[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2 \right]}$$

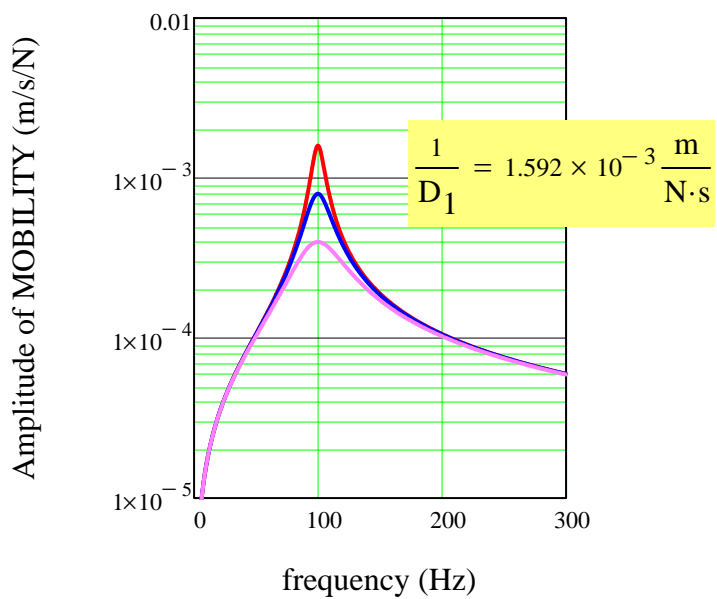
force/velocity

Mobility function

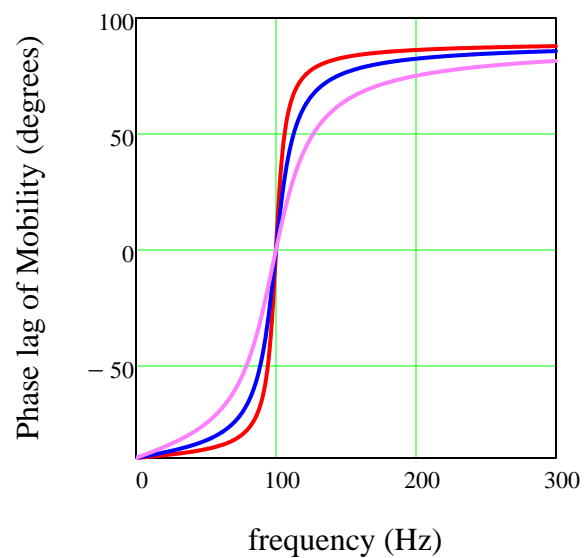
$$\frac{V_A}{F_O}$$

$$\text{Mob}(r, \zeta) := \frac{r \cdot \omega_n \cdot K^{-1}}{\sqrt{\left[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2 \right]}}$$

$$\varphi(r, \zeta) := \begin{cases} \varphi \leftarrow \text{atan} \left(\frac{2 \cdot \zeta \cdot r}{1 - r^2} \right) \cdot \left(\frac{180}{\pi} \right) \\ \varphi \leftarrow \varphi + 180 \text{ if } r > 1 \\ \varphi \leftarrow \varphi - 90 \end{cases}$$



- Xsi1=0.05
- Xsi2=2 x Xsi1
- Xsi3=2 x Xsi2



- Xsi1=0.05
- Xsi2=2 x Xsi1
- Xsi3=2 x Xsi2

Other times the **acceleration** is measured rather than the displacement or velocity, hence from

$$X(t) = Z \cdot e^{i \cdot \omega \cdot t}$$

obtain

$$A_X(t) = Z \cdot i^2 \cdot \omega^2 \cdot e^{i \cdot \omega \cdot t} = -\omega^2 \cdot Z \cdot e^{i \cdot (\omega \cdot t)} = a_A \cdot e^{i \cdot (\omega \cdot t - \varphi_A)}$$

and the **amplitude of the transfer function (acceleration/force)** is

$$\frac{a_A}{F_0} = \frac{\omega^2 \cdot M^{-1}}{\sqrt{[(K - M \cdot \omega^2)^2 + (\omega \cdot D)^2]}}$$

and $\varphi_A = \varphi - \pi$

Using the nat. frequency and damping ratio (ω_n, ζ) gives

**Accelerance fn
Inertance fn.**

$$\frac{a_A}{F_0} = \frac{r^2 \cdot M^{-1}}{\sqrt{[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2]}}$$

acceleration/force units of 1/M

While the

**APPARENT Mass or
Dynamic Mass fn:**

$$\frac{F_0}{a_A} = \frac{M}{r^2} \cdot \sqrt{[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2]}$$

Accelerance function

$$\frac{A_A}{F_O}$$

$$\text{Accel}(r, \zeta) := \frac{r^2 \cdot M^{-1}}{\sqrt{\left[(1 - r^2)^2 + (2 \cdot \zeta \cdot r)^2 \right]}}$$

$$\varphi(r, \zeta) := \begin{cases} \varphi \leftarrow \text{atan} \left(\frac{2 \cdot \zeta \cdot r}{1 - r^2} \right) \cdot \left(\frac{180}{\pi} \right) \\ \varphi \leftarrow \varphi + 180 \text{ if } r > 1 \\ \varphi \leftarrow \varphi - 180 \end{cases}$$

