

TWO DOF SYSTEM: Identification of system parameters (K,C,M) using IVF method.

LSA/04/08 revised 11/09

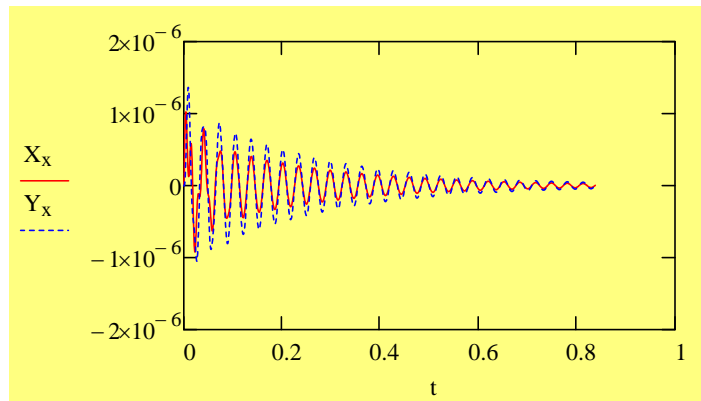
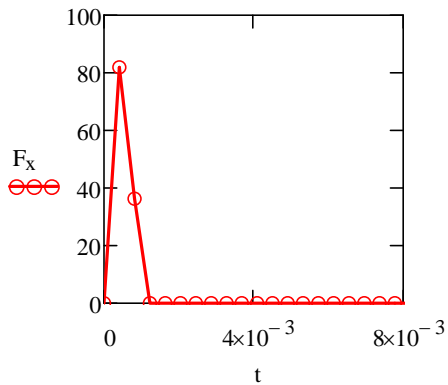
a. Read time domain data files:

Response obtained from Impact_response.mcd

transfer data

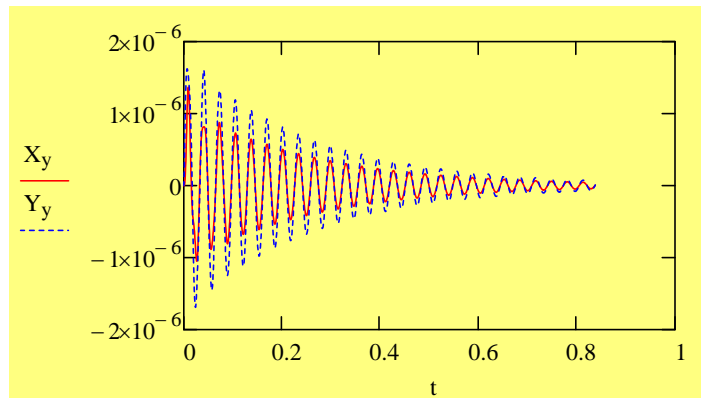
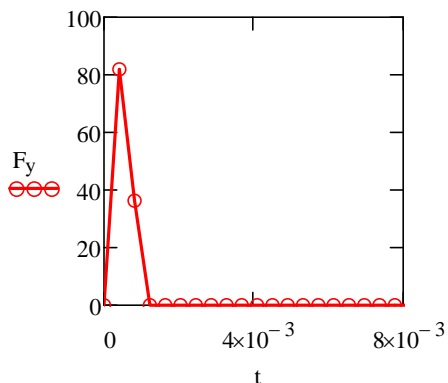
Plot excitation force in X dir. and responses X_x , Y_x versus time

Note time scale differences in load and displacements graphs



Plot excitation force in Y dir. and responses X_y , Y_y versus time

$N_t = 2.05 \times 10^3$ number of points



$$\frac{1}{\Delta T} = 2.44 \times 10^3$$

SAMPLING RATE

max(t) = 0.84

MAX time

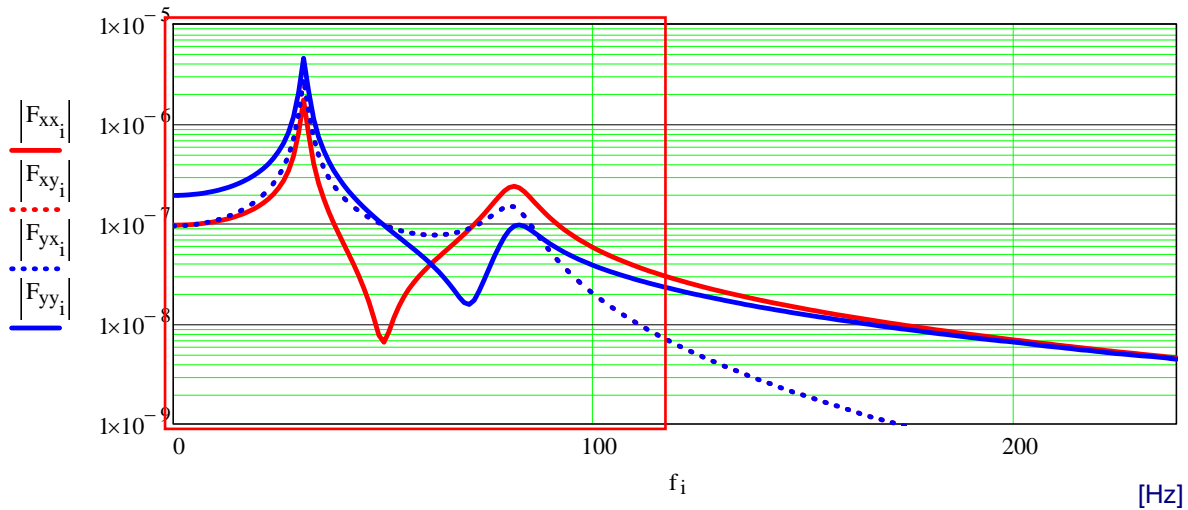
b. Transform forces and displacements to the frequency domain:

Select max index for identification:

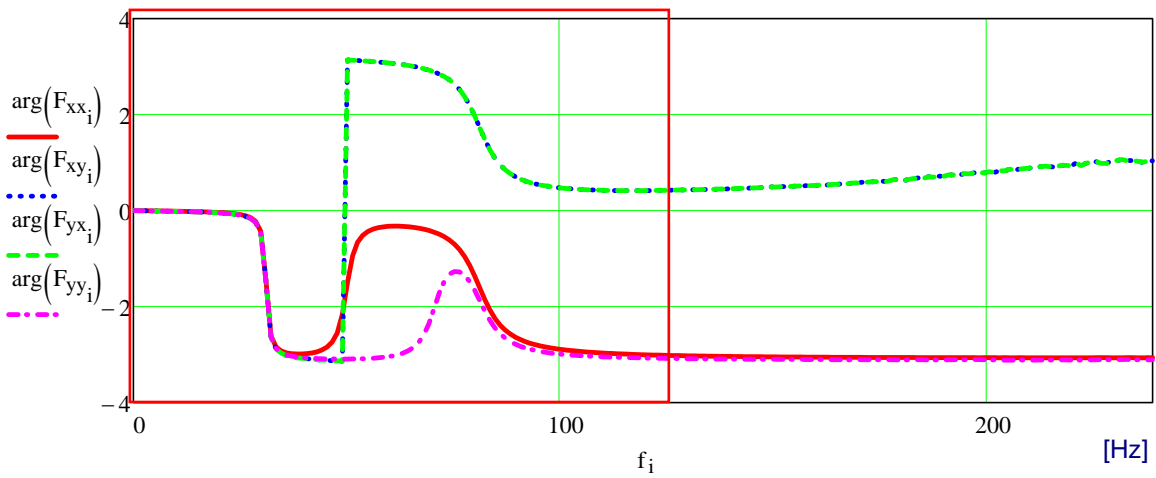
$$\text{Max} := 200 < \frac{N_t}{2} = 1.024 \times 10^3$$

System Flexibilities (amplitude)

$f_{Max} = 238.59$ Hz for identification range



System Flexibilities (phase)



Select the frequency range for the identification of parameters:

initial point: $i_o := 5$ Corresponding to: $f_{i_o} = 5.96$ Hz Max = 200
 final point: $i_f := \frac{\text{Max}}{2}$ $f_{i_f} = 119.3$ Hz

1. IMPEDANCE method:



$i := i_o..i_f$ Sweep over frequencies $f_{i_o} := f_{i_o}$ $f_{i_f} := f_{i_f}$

$w_i := \omega_i$

$w2_i := (\omega_i)^2$

Extract Real and Imaginary parts (only those in frequency range selected):

$H_{Rxxm_i} := (\text{Re}(H_{xx_i}))$ $H_{Ryxm_i} := (\text{Re}(H_{yx_i}))$ $H_{Ixxm_i} := (\text{Im}(H_{xx_i}))$ $H_{Iyxm_i} := (\text{Im}(H_{yx_i}))$
 $H_{Rxym_i} := (\text{Re}(H_{xy_i}))$ $H_{Ryyi} := (\text{Re}(H_{yy_i}))$ $H_{Ixym_i} := (\text{Im}(H_{xy_i}))$ $H_{Iyyi} := (\text{Im}(H_{yy_i}))$

Determine PARAMETERS from curve fits to impedances over frequency range selected

$k_{xx} := \text{intercept}(w2, H_{Rxxm})$ $k_{xy} := \text{intercept}(w2, H_{Rxy})$
 $k_{yx} := \text{intercept}(w2, H_{Ryxm})$ $k_{yy} := \text{intercept}(w2, H_{Ryy})$
 $m_{xx} := -\text{slope}(w2, H_{Rxxm})$ $m_{xy} := -\text{slope}(w2, H_{Rxy})$
 $m_{yx} := -\text{slope}(w2, H_{Ryxm})$ $m_{yy} := -\text{slope}(w2, H_{Ryy})$
 $c_{xx} := \text{slope}(w, H_{Ixxm})$ $c_{xy} := \text{slope}(w, H_{Ixym})$
 $c_{yx} := \text{slope}(w, H_{Iyxm})$ $c_{yy} := \text{slope}(w, H_{Iyy})$

$\text{Re}(H) = K - M \cdot \omega^2$

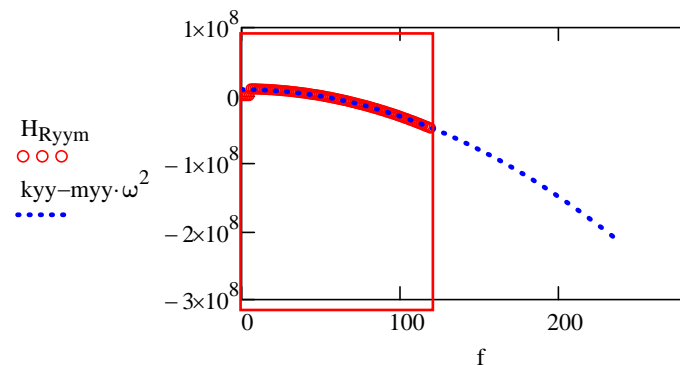
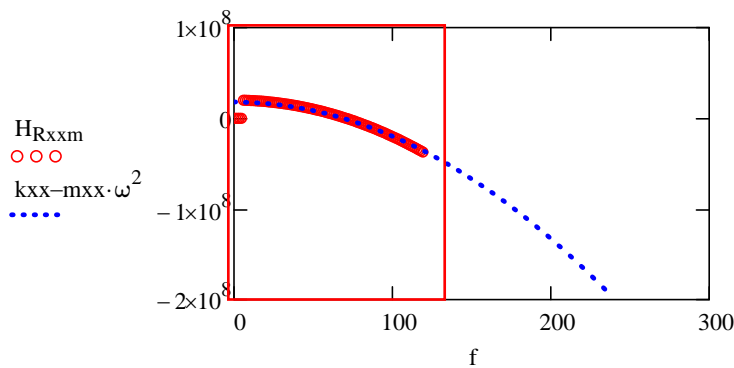
$\text{Ima}(H) = \omega \cdot C$

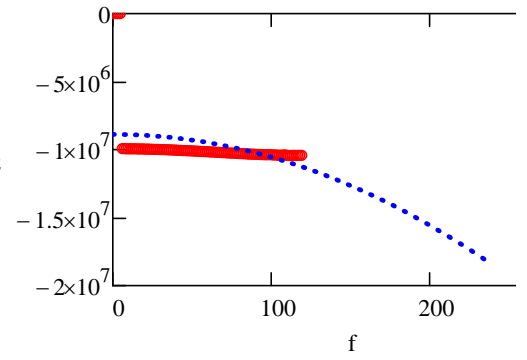
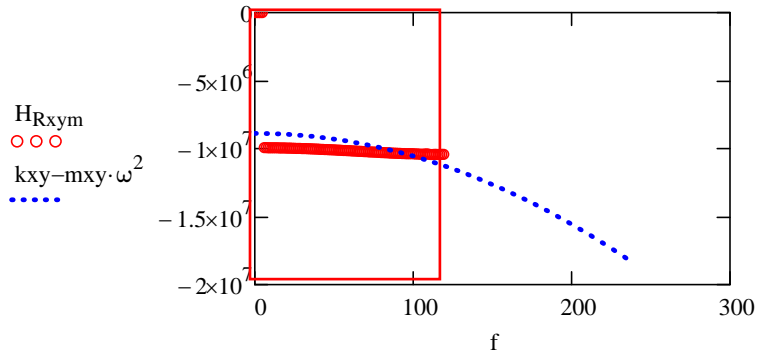
Make matrices of parameters $K_I := \begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \end{pmatrix}$ $C_I := \begin{pmatrix} c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix}$ $M_I := \begin{pmatrix} m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \end{pmatrix}$

REAL PARTS

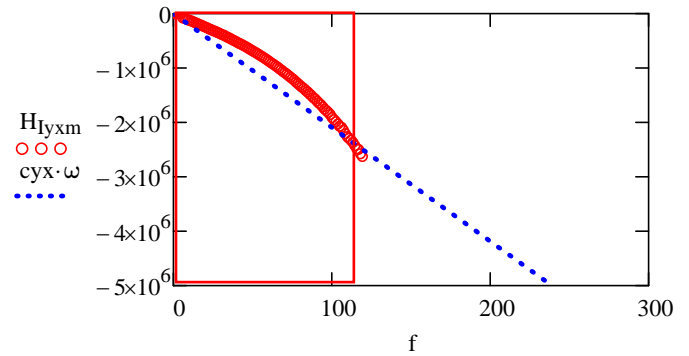
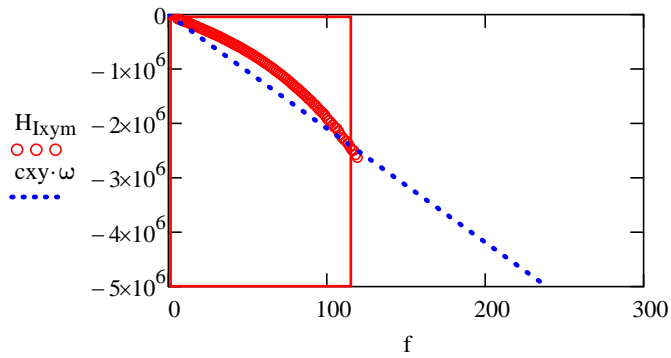
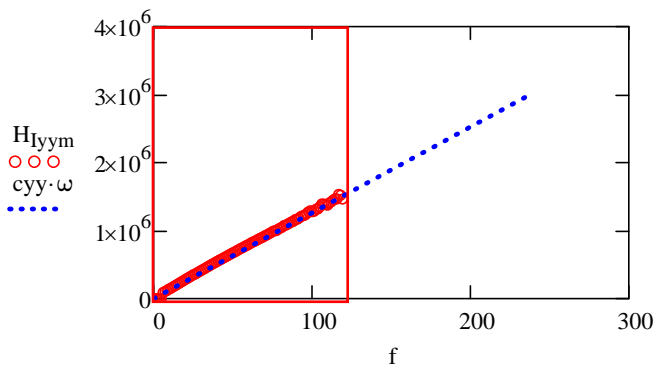
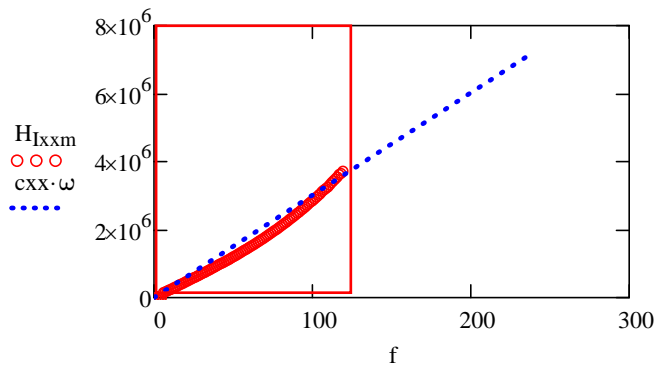
$f_{i_o} = 5.96$ Hz $f_{i_f} = 119.3$ Hz

SYMBOLS: data, LINE: CURVE FIT





IMAGINARY parts



Identified force coefficients over freq range:

$$f_{i0} = 5.96 \quad \text{to} \quad f_{if} = 119.3 \quad \text{Hz}$$

Compare to **ACTUAL** parameters

$$K_I = \begin{pmatrix} 1.79 \times 10^7 & -8.88 \times 10^6 \\ -8.88 \times 10^6 & 8.99 \times 10^6 \end{pmatrix} \quad \text{N/m}$$

$$M_I = \begin{pmatrix} 95.38 & 4.23 \\ 4.23 & 99.67 \end{pmatrix} \quad \text{kg}$$

$$C_I = \begin{pmatrix} 4794.2 & -3330.4 \\ -3330.4 & 2008.6 \end{pmatrix} \quad \text{Ns/m}$$

$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := \begin{pmatrix} 2 \cdot 10^7 & -1 \cdot 10^7 \\ -1 \cdot 10^7 & 1 \cdot 10^7 \\ 100 & 0 \\ 0 & 100 \\ 4500 & -2500 \\ -2500 & 2500 \end{pmatrix}$$

2) LEAST SQUARES METHOD

Construct a vector whose elements are the flexibility matrices at each frequency (each element of the vector is a matrix):

$$i := i_0..i_f$$

$$F_i := \begin{pmatrix} H_{xx,i} & H_{xy,i} \\ H_{yx,i} & H_{yy,i} \end{pmatrix}^{-1}$$

Now, the problem to solve is:

$$F \cdot H = I + E$$

where F are the measured flexibilities, H the approximated impedances, I the identity matrix, and E the error to be minimized.

The left hand side can be rearranged as:

$$A \cdot \begin{pmatrix} k \\ m \\ c \end{pmatrix} = I + E'$$

Now, the equations of each frequency decomposed into real and imaginary part. Stacking all the equations renders an undetermined system of equations (more equations than unknowns) of the same form, where:

A (as a function of the flexibilities) is given by:

```

a(F) :=
|
| A ← Re Fi0 ·  $\begin{bmatrix} 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} & 0 \\ 0 & 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} \end{bmatrix}$ 
|
| A ← stack(A, Im Fi0 ·  $\begin{bmatrix} 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} & 0 \\ 0 & 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} \end{bmatrix}$ 
|
| for i ∈ i0 + 1 .. if
|
|   | A ← stack(A, Re Fi ·  $\begin{bmatrix} 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i & 0 \\ 0 & 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i \end{bmatrix}$ 
|   |
|   | A ← stack(A, Im Fi ·  $\begin{bmatrix} 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i & 0 \\ 0 & 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i \end{bmatrix}$ 
|   |
| A

```

<= A = real part of the first frequency

<= stacks what was on A with the imaginary part of the first frequency

<= for loop from the second to the last frequencies.

<= stacks to A the real part of the ith frequency

<= stacks to A the imaginary part of the ith frequency

<= returns the matrix A

Auxiliary matrix of zeros [2x2]: zero_{1,1} := 0

The right hand side of the equation is given by:

```

I :=
|
| I ← identity(2)
|
| I ← stack(I, zero)
|
| for i ∈ i0 + 1 .. if
|
|   | I ← stack(I, identity(2))
|   |
|   | I ← stack(I, zero)
|   |
| I

```

The least squares solution of the problem (minimum E) is:

$\underline{A} := a(F)$ <= Matrix A for the measured flexibilities

$$q_1 := (A^T \cdot A)^{-1} \cdot A^T \cdot I$$

$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := q_1$$

$$q_1 = \begin{pmatrix} 2.01 \times 10^7 & -10 \times 10^6 \\ -9.99 \times 10^6 & 1.01 \times 10^7 \\ 101.92 & 1.16 \\ 1.15 & 103.13 \\ 4365.36 & -2434.94 \\ -2426.08 & 2447.98 \end{pmatrix}$$

Estimated system parameters based on least squares fit to flexibilities

$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := \begin{pmatrix} 2 \cdot 10^7 & -1 \cdot 10^7 \\ -1 \cdot 10^7 & 1 \cdot 10^7 \\ 100 & 0 \\ 0 & 100 \\ 4500 & -2500 \\ -2500 & 2500 \end{pmatrix}$$

Actual values:

3. Instrumental variable method



$$q = \begin{pmatrix} 2 \times 10^7 & -10 \times 10^6 \\ -10 \times 10^6 & 1 \times 10^7 \\ 101.9 & 1.1 \\ 1.1 & 103.1 \\ 4366.4 & -2435.6 \\ -2426.8 & 2448.5 \end{pmatrix}$$

Actual values:

$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := \begin{pmatrix} 2 \cdot 10^7 & -1 \cdot 10^7 \\ -1 \cdot 10^7 & 1 \cdot 10^7 \\ 100 & 0 \\ 0 & 100 \\ 4500 & -2500 \\ -2500 & 2500 \end{pmatrix}$$



4. Build output/input (transfer functions)

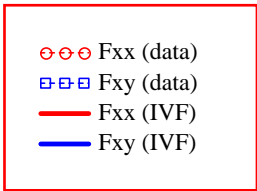
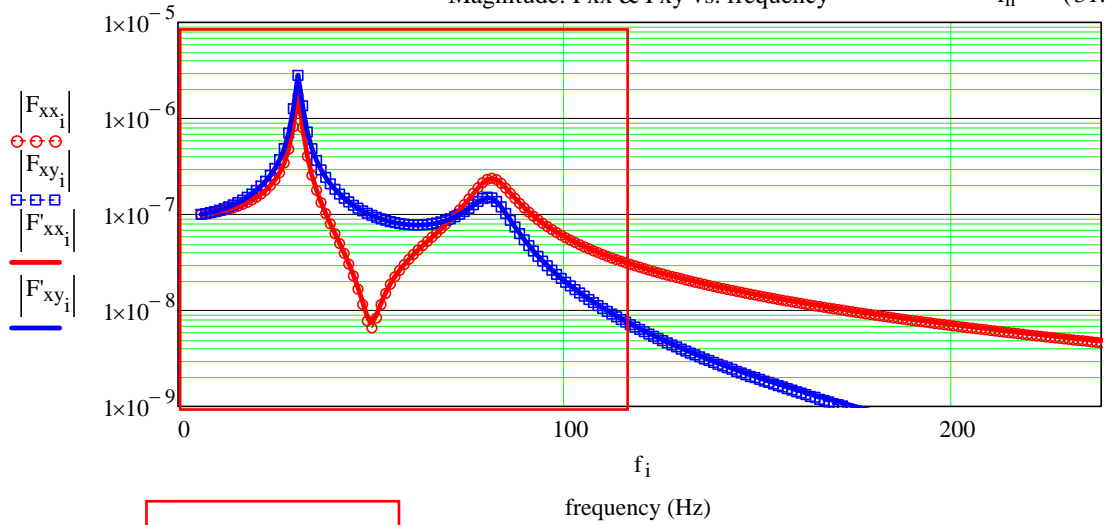
FLEXIBILITY functions - data and IVF



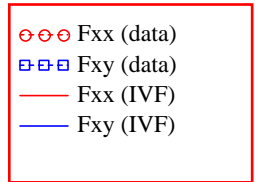
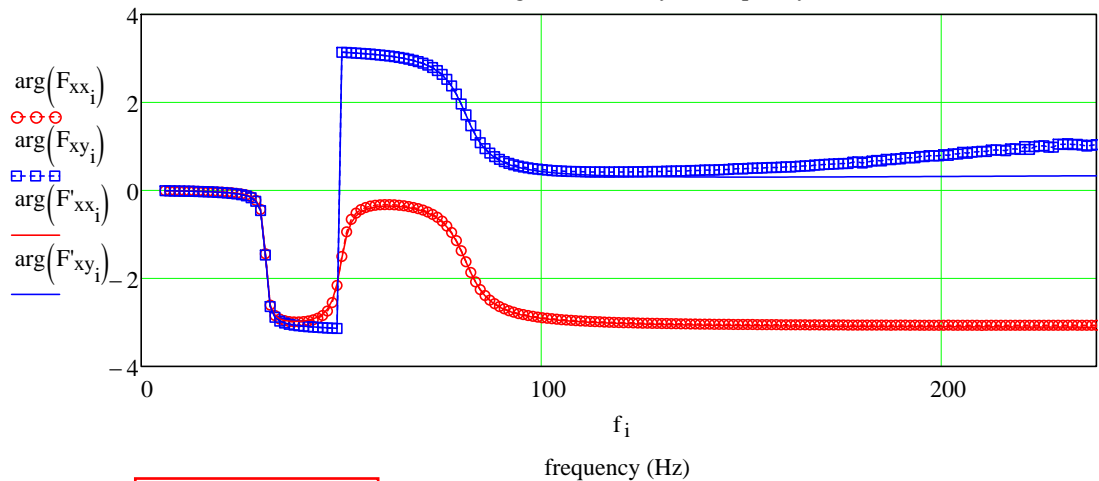
Magnitude: Fxx & Fxy vs. frequency

$f_n^T = (31.08 \ 81.13) \text{ Hz}$

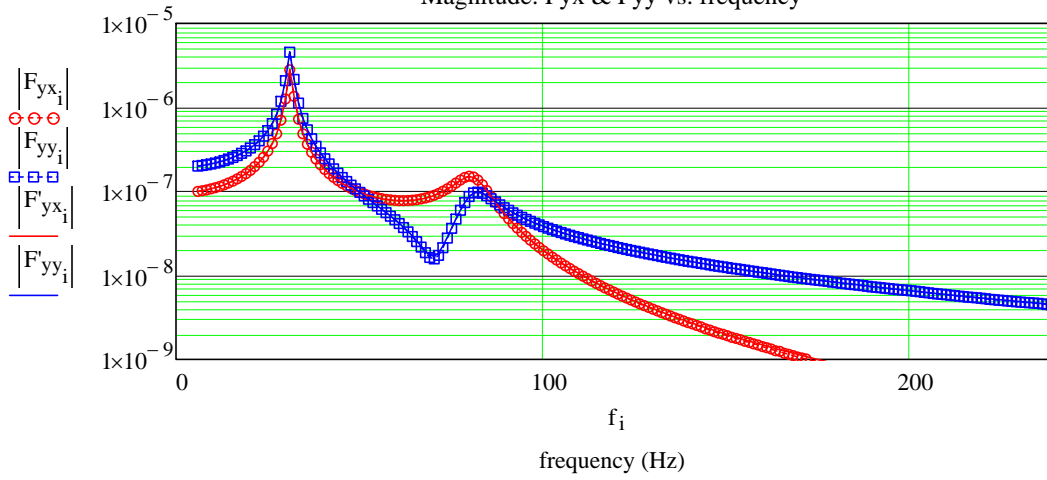
SYMBOLS DATA
LINES IVF results



Phase angle: Fxx & Fxy vs frequency

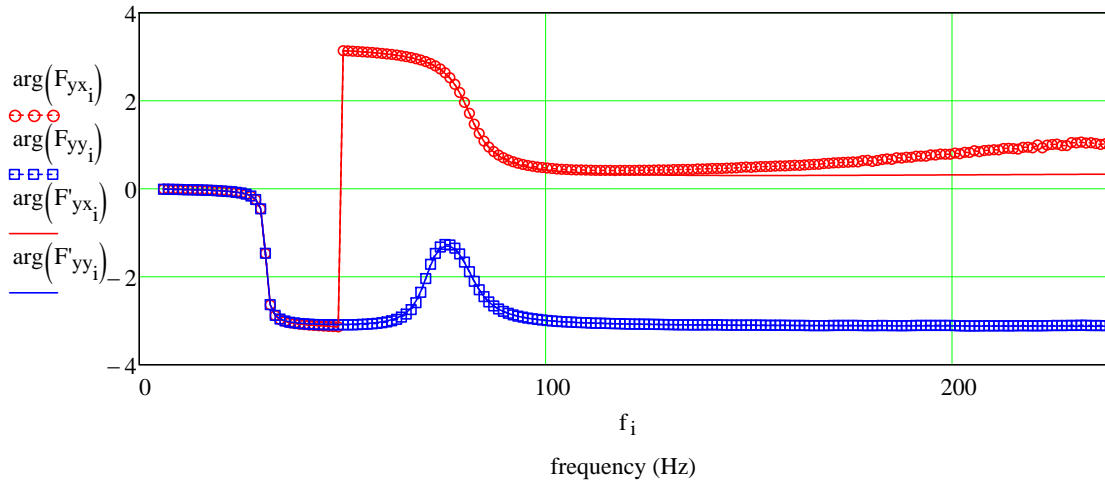


Magnitude: Fyx & Fyy vs. frequency



- Fyx (data)
- Fyy (data)
- Fyy(IVF)
- Fyy (IVF)

Phase angle: Fyx & Fyy vs frequency



- Fyx (data)
- Fyy (data)
- Fyx (IVF)
- Fyy (IVF)