

DRAWINGS NOT TO SCALE

The figure shows a pendulum-like arrangement for measuring the radius of gyration (k) of a rotor (i.e. polar mass moment of inertia $I_p = m k^2$). The rotor is suspended from massless and inextensible wires. Each wire of length (a) is fixed at radius (b) from the rotor center of mass. From small amplitude motions $\theta(t)$, the procedure requires recording the natural period of motion and then extracts the radius of gyration from a simple engineering formula.

- a) **Clearly outlining** physical considerations and assumptions **DERIVE** the equation of motion for the arrangement shown, i.e. $I_p \ddot{\theta} + K_\theta \theta = 0$, where $K_\theta = W (b^2/a)$ is a torsional “stiffness” depending on the wires’ length and disposition and the rotor weight.

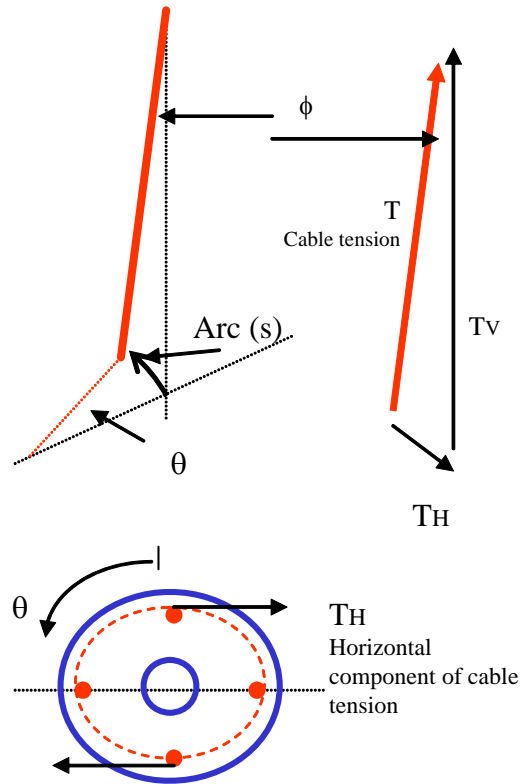
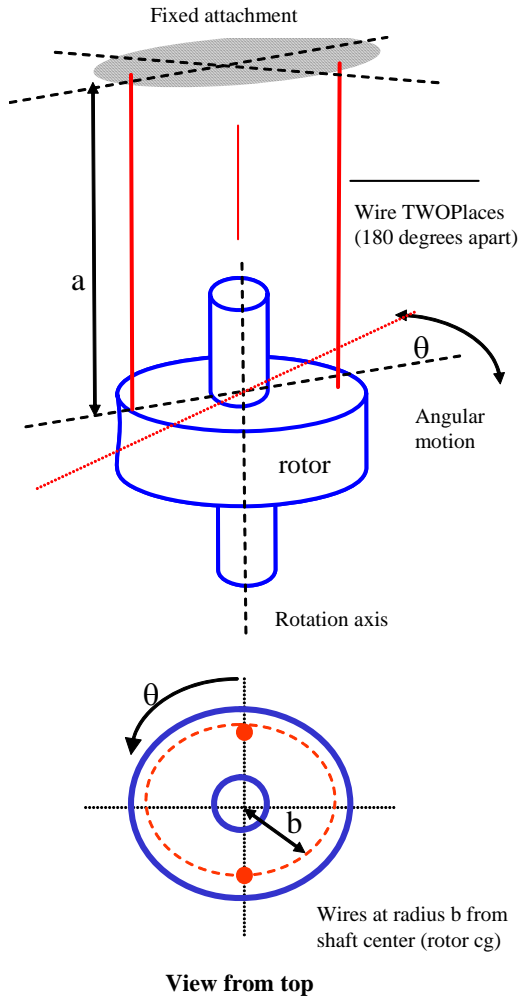
Show a rigorous procedure, define variables, establish principles used, note assumptions, and highlight steps in modeling and analysis.

- b) Measurements were conducted with a single stage compressor rotor. The rotor weighs 150 lb_f, and $a = 100$ inch, $b = 10$ inch. The rotor performed 10 oscillations in 30 seconds. Determine, the system natural frequency [rad/s], the rotor polar mass moment of inertia I_p [lb_f-inch-s²], and the radius of gyration k [inch]

NOTE: Neatness, organization, explanations in complete sentences, and clarity of procedure are a must for full grade.

QUIZ 10

Determining mass moments of inertia



Kinematics and FBD of rotor for angular motions

Constraint: arc length $s = \phi a = \theta b$

Assumptions :

no friction, small angular motions, rotations about cg, cables are massless and inextensible.

Let: $\theta'' = \frac{d^2}{dt^2} \theta$

kinematic constraint:

arc motion (s) described by rotor motion is given by

$s = a \cdot \phi = b \cdot \theta$ [1]

with ϕ as the angle between a support cable and the vertical plane

For small angular motions $\theta(t)$ about the center of mass, the equation of motion is

$I_P \cdot \theta'' = -2T_H \cdot b$ [2] where T_H is the component of the cable tension in the horizontal plane

from the EOM for vertical motions of rotor cg: $M \cdot y'' = 2 \cdot T_V - W$ [3]

where T_V is the component of the cable tension in the vertical plane

For small amplitude angular motions. From [1], $\phi = \frac{b}{a} \cdot \theta$ [4a] and: $y'' := 0$

.Thus,

$$T_V := \frac{W}{2} \quad \text{and} \quad T_H = T_V \cdot \frac{\sin\phi}{\cos\phi} = \frac{W}{2} \cdot \frac{b}{a} \cdot \theta \quad [4b]$$

Substitution of [4b] into [2] renders the desired EOM:

$$I_P \cdot \theta'' + k_\theta \cdot \theta = 0 \quad [6a] \quad \text{where} \quad k_\theta = W \cdot \frac{b^2}{a}$$

since: $W := m \cdot g$ and $I_P = m \cdot r_k^2$

$$\text{. Then [6a] reduces to:} \quad \theta'' + g \cdot \frac{b^2}{a \cdot r_k^2} \cdot \theta = 0 \quad [6b]$$

The natural frequency of the oscillatory system is defined as: $\omega_n = \left(\frac{k_\theta}{I_P} \right)^{.5} \quad [7]$

and the natural period of motion is: $T_n = \frac{2 \cdot \pi}{\omega_n}$

(b) Engineering calculations

$$T_n := \frac{30}{10} \cdot s \quad \omega_n := \frac{2 \cdot \pi}{T_n} \quad \omega_n = 2.094 \frac{\text{rad}}{\text{s}}$$

$$a := 100 \cdot \text{in} \quad W := 150 \cdot \text{lb}$$

$$b := 10 \cdot \text{in}$$

$$k_\theta := W \cdot \frac{b^2}{a} \quad k_\theta = 150 \text{ lb} \cdot \text{in} \quad \text{stiffness}$$

$$\text{from [7], the polar moment of inertia is} \quad I_P := \frac{k_\theta}{\omega_n^2} \quad I_P = 34.196 \text{ lb} \cdot \text{in} \cdot \text{s}^2$$

$$\text{and the radius of gyration is} \quad r_k := \left(\frac{I_P \cdot g}{W} \right)^{.5} \quad r_k = 9.382 \text{ in}$$

The equation of motion can be easily derived using conservation of mechanical energy:

$$T = \frac{1}{2} \cdot I_P \cdot \left(\frac{d}{dt} \theta \right)^2 \quad \text{kinetic energy}$$

$$V = m \cdot g \cdot h \quad \text{change in potential energy}$$

$$h = a \cdot (1 - \cos(\phi)) = a \cdot \frac{\phi^2}{2}$$

for small angles, and $\phi = \frac{b}{a} \cdot \theta$

Thus, $V = m \cdot g \cdot \frac{b^2}{a} \cdot \frac{\theta^2}{2} = \frac{1}{2} \cdot k_\theta \cdot \theta^2$ where $k_\theta = W \cdot \frac{b^2}{a}$

Hence from $\frac{d}{dt}(T + V) = 0$ $I_P \cdot \frac{d^2}{dt^2} \theta + k_\theta \cdot \theta = 0$