

MDOF: PERIODIC FORCED RESPONSE

ORIGIN := 1

Consider the n-DOF system governed by

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$$M \cdot \frac{d^2}{dt^2} X + C \cdot \frac{d}{dt} X + K \cdot X = F(t) = F_0 \cdot \cos(\Omega \cdot t) \quad (1)$$

where X is a vector of n-displacements, F is a vector of periodic forces with frequency Ω . M, C, K are $n \times n$ matrices of inertia, damping and stiffness coefficients..

$$X = \{x_1, x_2, \dots, x_n\}^T \quad F = \{F_1, F_2, \dots, F_n\}^T$$

The force vector acts on the system over a long-long-long time. Hence, transient response effects have died and the periodic forced response of the system is

$$X = X_c \cdot \cos(\Omega \cdot t) + X_s \cdot \sin(\Omega \cdot t) \quad (2)$$

where X_c and X_s are vectors of displacements associated to the cos & sine terms. Note that

$$\frac{d}{dt} X = -X_c \cdot \Omega \cdot \sin(\Omega \cdot t) + X_s \cdot \Omega \cdot \cos(\Omega \cdot t) \quad (3)$$

$$\frac{d^2}{dt^2} X = -\Omega^2 \cdot X = -X_c \cdot \Omega^2 \cdot \cos(\Omega \cdot t) - X_s \cdot \Omega^2 \cdot \sin(\Omega \cdot t)$$

Substitution of Eqs. (2) and (3) into Eq. (1) gives

$$\begin{aligned} & (K - \Omega^2 \cdot M) \cdot X_c \cdot \cos(\Omega \cdot t) + X_s \cdot \Omega \cdot C \cdot \cos(\Omega \cdot t) \\ & + X_c \cdot \Omega \cdot C \cdot \sin(\Omega \cdot t) + (K - \Omega^2 \cdot M) \cdot X_s \cdot \sin(\Omega \cdot t) = F_0 \cdot \cos(\Omega \cdot t) \end{aligned} \quad (4)$$

The functions cos & sin are linearly independent. Hence, collecting similar terms we have

$$\begin{aligned} & (K - \Omega^2 \cdot M) \cdot X_c + C \cdot \Omega \cdot X_s = F_0 \\ & -C \cdot \Omega \cdot X_c + [(K - \Omega^2 \cdot M) \cdot X_s] = 0 \end{aligned} \quad (5)$$

Eqns. (5) are written in matrix form as

$$\begin{pmatrix} K - \Omega^2 \cdot M & \Omega \cdot C \\ -\Omega \cdot C & K - \Omega^2 \cdot M \end{pmatrix} \cdot \begin{pmatrix} X_c \\ X_s \end{pmatrix} = \begin{pmatrix} F_o \\ 0 \end{pmatrix} \quad (6)$$

← For n=2 (DOF)

This is a system of 4-equations with 4-unknowns which can be easily solved for any particular frequency (Ω)

Example:

$$\text{let } M := \begin{pmatrix} 2.381 \times 10^3 & -113.398 \\ -113.398 & 566.99 \end{pmatrix} \cdot \text{kg} \quad F_o := \begin{pmatrix} 10^4 \\ 0 \end{pmatrix} \cdot \text{N}$$

$$K := \begin{pmatrix} 1.226 \times 10^8 & -3.503 \times 10^7 \\ -3.503 \times 10^7 & 3.503 \times 10^7 \end{pmatrix} \cdot \frac{\text{N}}{\text{m}}$$

$$C := \begin{pmatrix} 10 & -2 \\ -3 & 3 \end{pmatrix} \cdot 4000 \cdot \frac{\text{N} \cdot \text{s}}{\text{m}}$$

Make matrix

$$G(\Omega) := \begin{pmatrix} K - \Omega^2 \cdot M & \Omega \cdot C \\ -\Omega \cdot C & K - \Omega^2 \cdot M \end{pmatrix}$$

$$G(\Omega) := \begin{pmatrix} K_{1,1} - \Omega^2 \cdot M_{1,1} & K_{1,2} - \Omega^2 \cdot M_{1,2} & \Omega \cdot C_{1,1} & \Omega \cdot C_{1,2} \\ K_{2,1} - \Omega^2 \cdot M_{2,1} & K_{2,2} - \Omega^2 \cdot M_{2,2} & \Omega \cdot C_{2,1} & \Omega \cdot C_{2,2} \\ -\Omega \cdot C_{1,1} & -\Omega \cdot C_{1,2} & K_{1,1} - \Omega^2 \cdot M_{1,1} & K_{1,2} - \Omega^2 \cdot M_{1,2} \\ -\Omega \cdot C_{2,1} & -\Omega \cdot C_{2,2} & K_{2,1} - \Omega^2 \cdot M_{2,1} & K_{2,2} - \Omega^2 \cdot M_{2,2} \end{pmatrix}$$

Find solution over a range of frequencies

$N := 100$

$$f_{\min} := 10 \cdot \text{Hz}$$

$$f_{\max} := 80 \cdot \text{Hz}$$

$$\Omega_{\min} := f_{\min} \cdot 2 \cdot \pi$$

$$\Omega_{\max} := f_{\max} \cdot 2 \cdot \pi$$

$$\Delta\Omega := \frac{(\Omega_{\max} - \Omega_{\min})}{N - 1}$$

$$j := 1..N$$

$$\Omega_j := \Omega_{\min} + \Delta\Omega \cdot j \quad \text{freq}_j := \frac{\Omega_j}{2 \cdot \pi}$$

Solve:

$$\begin{pmatrix} X_{1c_j} \\ X_{2c_j} \\ X_{1s_j} \\ X_{2s_j} \end{pmatrix} := G(\Omega_j)^{-1} \cdot \begin{pmatrix} F_{o1} \\ F_{o2} \\ 0 \\ 0 \end{pmatrix}$$

force cos terms

force sin terms

for example, the response for DOF#1 is

$$X_1(t) = X_{1c} \cdot \cos(\Omega \cdot t) + X_{1s} \cdot \sin(\Omega \cdot t)$$

which can also be written as

$$X_1(t) = A_1 \cdot \cos(\Omega \cdot t + \phi_1)$$

where A_1 and ϕ_1 denote the amplitude and phase lag of the response

Hence, define for each DOF:

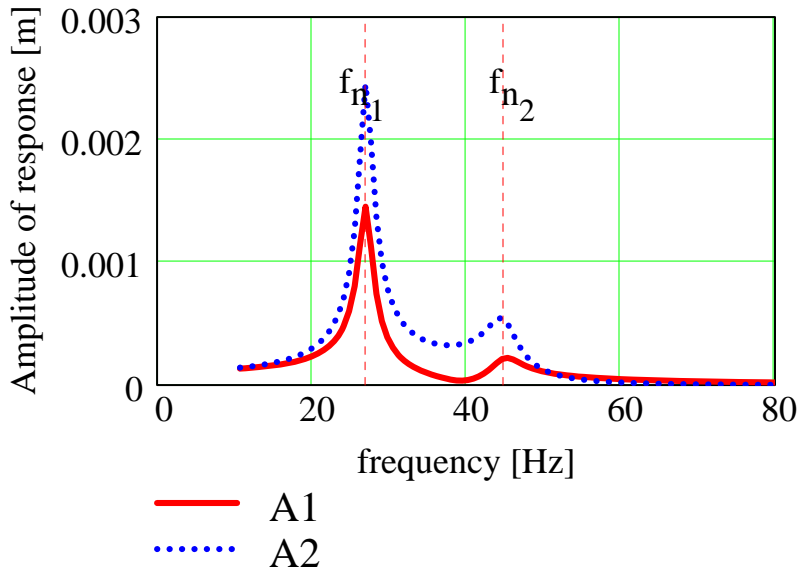
$$A_{1j} := \left[(X_{1c_j})^2 + (X_{1s_j})^2 \right]^{.5}$$

$$\phi_{1j} := -\text{atan} \left(\frac{X_{1s_j}}{X_{1c_j}} \right) \cdot \frac{180}{\pi}$$

$$A_{2j} := \left[(X_{2c_j})^2 + (X_{2s_j})^2 \right]^{.5}$$

$$\phi_{2j} := -\text{atan} \left(\frac{X_{2s_j}}{X_{2c_j}} \right) \cdot \frac{180}{\pi}$$

PLOTS of the FRF: amplitude and phase angle of the system periodic response



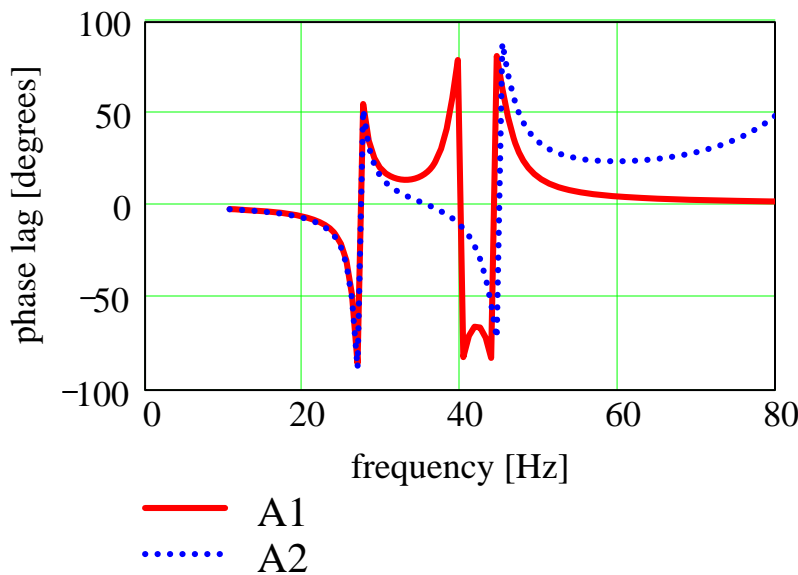
undamped natural freqs.

$$f_n = \begin{pmatrix} 27.019 \\ 44.903 \end{pmatrix} \text{ Hz}$$

Questions from analysis:

IS RESPONSE SAFE?

AT WHICH FREQUENCIES SYSTEM OPERATION MUST BE AVOIDED?



Find UNDAMPED natural frequencies and mode shapes

$$\text{let: } E := M^{-1} \cdot K$$

$$\lambda := \text{eigenvals}(E)$$

$$f_n := \frac{\lambda^{.5}}{2 \cdot \pi}$$

$$f_n = \begin{pmatrix} 27.019 \\ 44.903 \end{pmatrix} \text{ Hz}$$

$$a_1 := \text{eigenvec}(E, \lambda_1) \quad a_2 := \text{eigenvec}(E, \lambda_2)$$

$$a_1 = \begin{pmatrix} 0.507 \\ 0.862 \end{pmatrix}$$

$$a_2 = \begin{pmatrix} -0.362 \\ 0.932 \end{pmatrix}$$

$$A := \text{augment}(a_1, a_2) \quad \text{MODAL matrix}$$

MODAL matrices

$$A^T \cdot M \cdot A = \begin{pmatrix} 934.399 & 5.387 \times 10^{-14} \\ 5.465 \times 10^{-14} & 881.457 \end{pmatrix} \text{ kg}$$

$$A^T \cdot K \cdot A = \begin{pmatrix} 2.693 \times 10^7 & 6.361 \times 10^{-9} \\ 1.252 \times 10^{-8} & 7.016 \times 10^7 \end{pmatrix} \frac{\text{kg}}{\text{s}^2}$$

$$A^T \cdot C \cdot A = \begin{pmatrix} 1.046 \times 10^4 & 2.258 \times 10^3 \\ -881.491 & 2.242 \times 10^4 \end{pmatrix} \frac{\text{kg}}{\text{s}}$$

Modal damping is NOT diagonal