

TWO DOF SYSTEM: Identification of system parameters (K,C,M) using IVF method.

LSA/04/08 revised 11/09

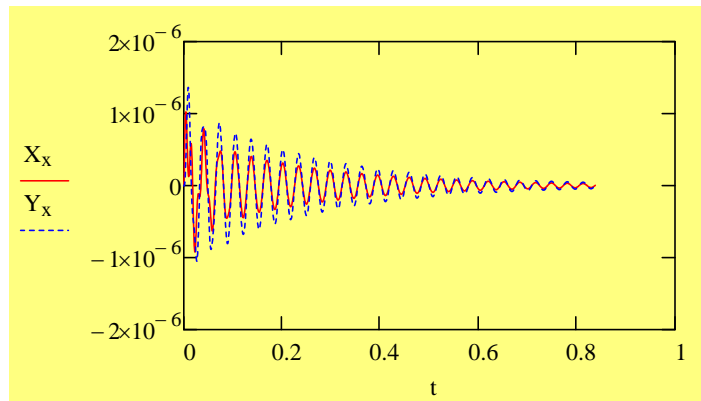
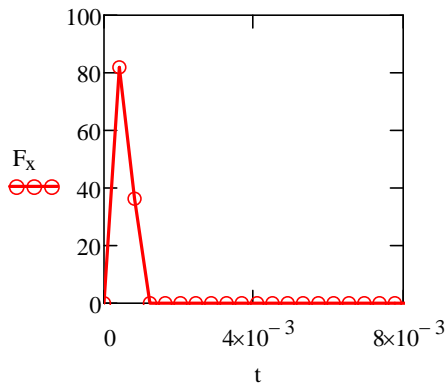
a. Read time domain data files:

Response obtained from Impact_response.mcd

transfer data

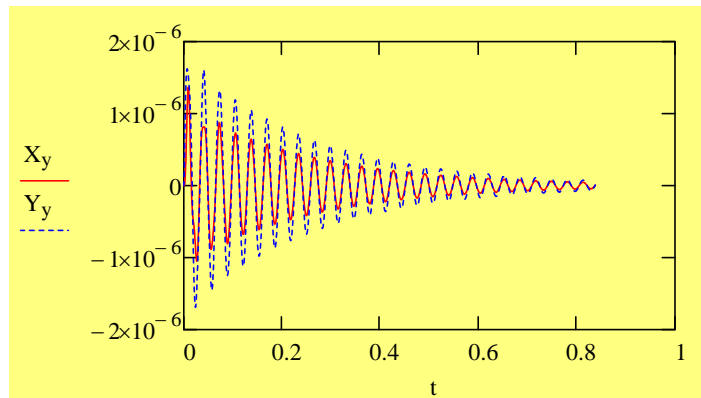
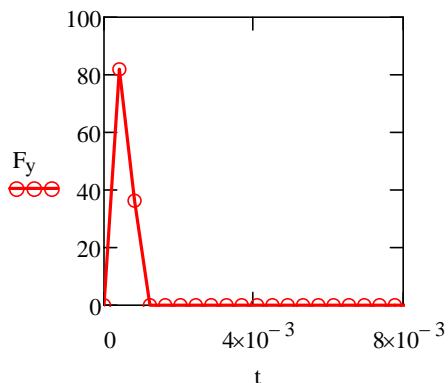
Plot excitation force in X dir. and responses Xx, Yx versus time

Note time scale differences in load and displacements graphs



Plot excitation force in Y dir. and responses Xy, Yy versus time

$N_t = 2.05 \times 10^3$ number of points



$$\frac{1}{\Delta T} = 2.44 \times 10^3$$

SAMPLING RATE

max(t) = 0.84

MAX time

b. Transform forces and displacements to the frequency domain:

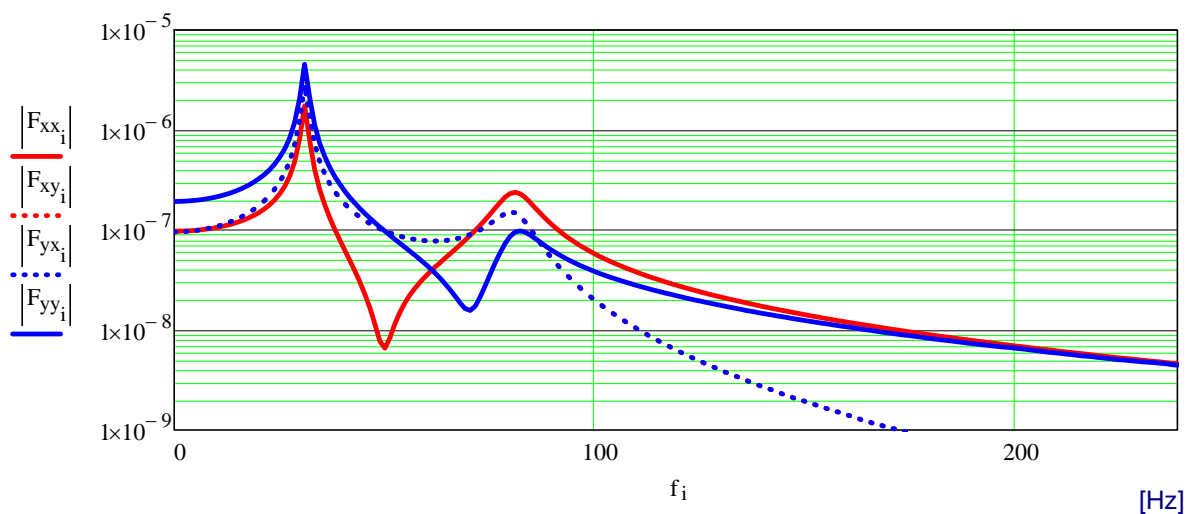
Select max index for identification:

Max := 200

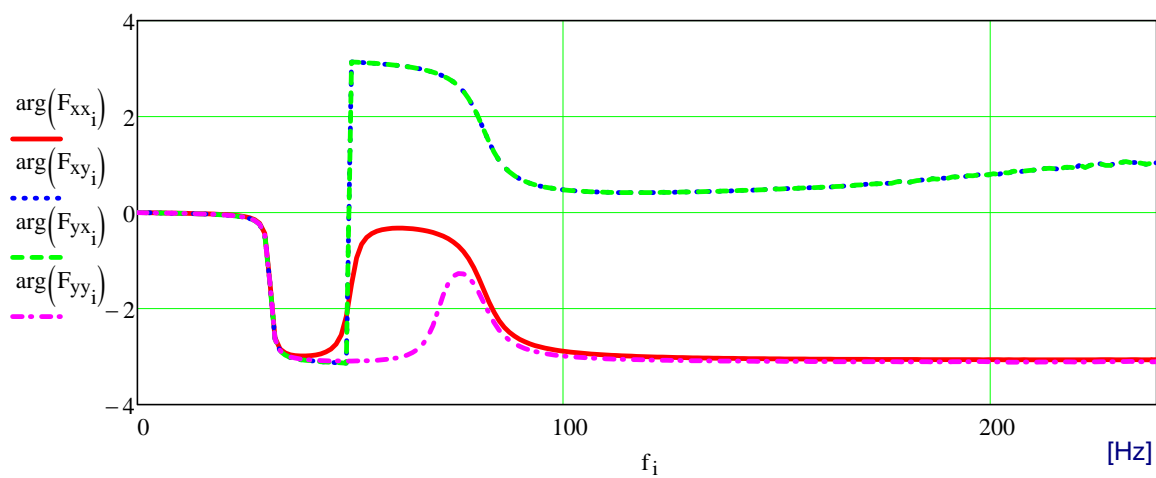
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$$\frac{N_t}{2} = 1.024 \times 10^3$$

System Flexibilities (amplitude)

 $f_{\text{Max}} = 238.59$ Hz for identification range

System Flexibilities (phase)



Select the frequency range for the identification of parameters:

initial point: $i_o := 5$ Corresponding to: $f_{i_o} = 5.96$ Hz Max = 200
 final point: $i_f := \frac{\text{Max}}{2}$ $f_{i_f} = 119.3$ Hz

1. IMPEDANCE method:



$i := i_o..i_f$ Sweep over frequencies $f_{i_o} := f_{i_o}$ $f_{i_f} := f_{i_f}$

$w_i := \omega_i$

$$w2_i := (\omega_i)^2$$

Extract Real and Imaginary parts (only those in frequency range selected):

$$\begin{aligned} H_{Rxxm_i} &:= \left(\text{Re}(H_{xx_i}) \right) & H_{Ryxm_i} &:= \left(\text{Re}(H_{yx_i}) \right) & H_{Ixxm_i} &:= \left(\text{Im}(H_{xx_i}) \right) & H_{Iyxm_i} &:= \left(\text{Im}(H_{yx_i}) \right) \\ H_{Rxym_i} &:= \left(\text{Re}(H_{xy_i}) \right) & H_{Ryym_i} &:= \left(\text{Re}(H_{yy_i}) \right) & H_{Ixym_i} &:= \left(\text{Im}(H_{xy_i}) \right) & H_{Iyym_i} &:= \left(\text{Im}(H_{yy_i}) \right) \end{aligned}$$

Determine PARAMETERS from curve fits to impedances over frequency range selected

$$\begin{aligned} k_{xx} &:= \text{intercept}(w2, H_{Rxxm}) & k_{xy} &:= \text{intercept}(w2, H_{Ryxm}) \\ k_{yx} &:= \text{intercept}(w2, H_{Ryym}) & k_{yy} &:= \text{intercept}(w2, H_{Ryym}) \\ m_{xx} &:= -\text{slope}(w2, H_{Rxxm}) & m_{xy} &:= -\text{slope}(w2, H_{Ryxm}) \\ m_{yx} &:= -\text{slope}(w2, H_{Ryxm}) & m_{yy} &:= -\text{slope}(w2, H_{Ryym}) \\ c_{xx} &:= \text{slope}(w, H_{Ixxm}) & c_{xy} &:= \text{slope}(w, H_{Ixym}) \\ c_{yx} &:= \text{slope}(w, H_{Iyxm}) & c_{yy} &:= \text{slope}(w, H_{Iyym}) \end{aligned}$$

$$\text{Re}(H) = K - M \cdot \omega^2$$

$$\text{Ima}(H) = \omega \cdot C$$

Make matrices of parameters

$$K_I := \begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \end{pmatrix}$$

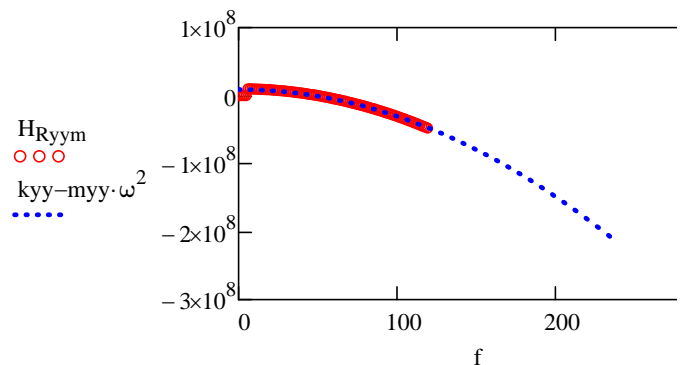
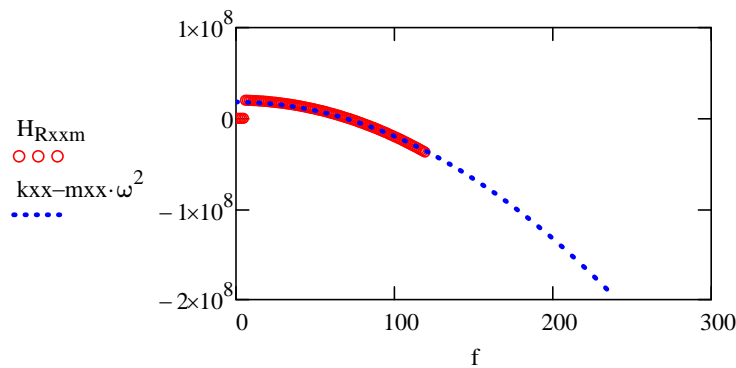
$$C_I := \begin{pmatrix} c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix}$$

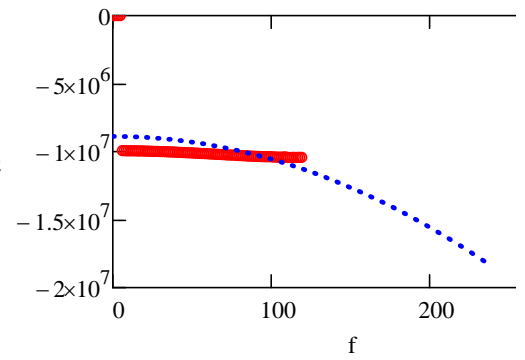
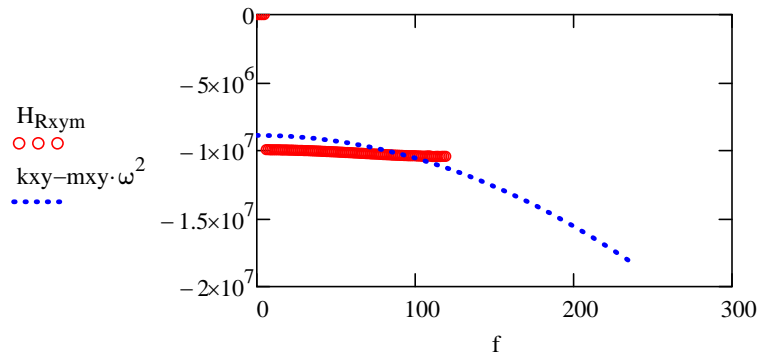
$$M_I := \begin{pmatrix} m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \end{pmatrix}$$

REAL PARTS

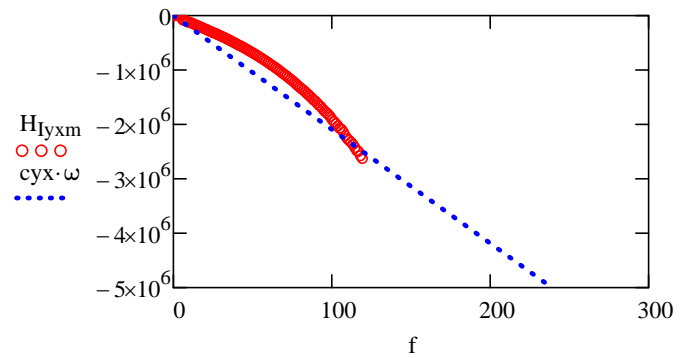
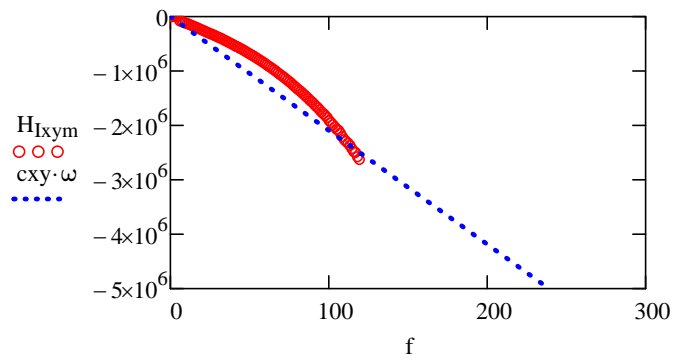
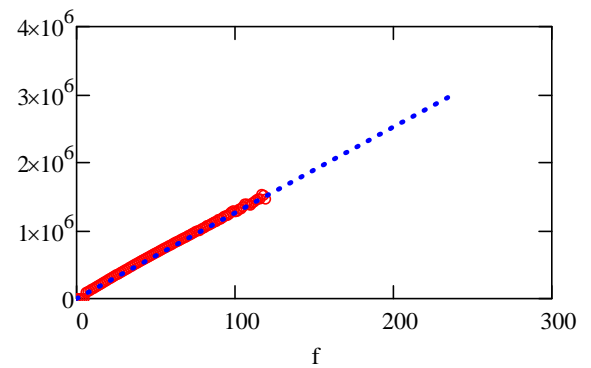
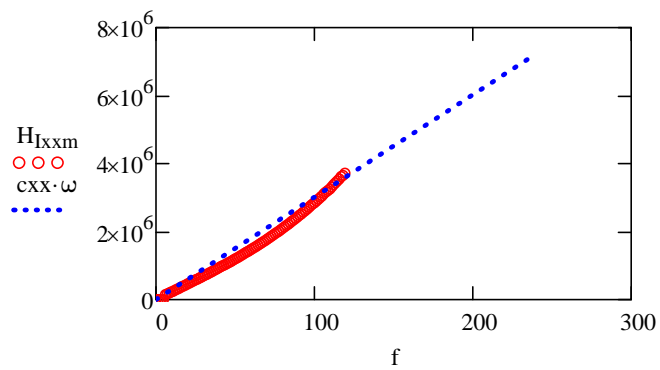
$f_{i_o} = 5.96$ Hz $f_{i_f} = 119.3$ Hz

SYMBOLS: data, LINE: CURVE FIT





IMAGINARY parts



Identified force coefficients over freq range:

$$f_{i0} = 5.96$$

$$\text{to } f_{if} = 119.3 \text{ Hz}$$

Compare to ACTUAL parameters

$$K_I = \begin{pmatrix} 1.79 \times 10^7 & -8.88 \times 10^6 \\ -8.88 \times 10^6 & 8.99 \times 10^6 \end{pmatrix} \quad \text{N/m}$$

$$M_I = \begin{pmatrix} 95.38 & 4.23 \\ 4.23 & 99.67 \end{pmatrix} \quad \text{kg}$$

$$C_I = \begin{pmatrix} 4794.2 & -3330.4 \\ -3330.4 & 2008.6 \end{pmatrix} \quad \text{Ns/m}$$

$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := \begin{pmatrix} 2 \cdot 10^7 & -1 \cdot 10^7 \\ -1 \cdot 10^7 & 1 \cdot 10^7 \\ 100 & 0 \\ 0 & 100 \\ 4500 & -2500 \\ -2500 & 2500 \end{pmatrix}$$

2) LEAST SQUARES METHOD



Construct a vector whose elements are the flexibility matrices at each frequency (each element of the vector is a matrix):

$$i := i_0 .. i_f$$

$$\underline{\underline{F}}_i := \begin{pmatrix} H_{xx_i} & H_{xy_i} \\ H_{yx_i} & H_{yy_i} \end{pmatrix}^{-1}$$

Now, the problem to solve is:

$$F \cdot H = I + E$$

where F are the measured flexibilities, H the approximated impedances, I the identity matrix, and E the error to be minimized.

The left hand side can be rearranged as:

$$A \cdot \begin{pmatrix} k \\ m \\ c \end{pmatrix} = I + E'$$

Now, the equations of each frequency decomposed into real and imaginary part. Stacking all the equations renders an undetermined system of equations (more equations than unknowns) of the same form, where:

A (as a function of the flexibilities) is given by:

$$a(F) := \left| \begin{array}{l} A \leftarrow \text{Re} \left[F_{i_0} \cdot \begin{bmatrix} 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} & 0 \\ 0 & 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} \end{bmatrix} \right] \\ A \leftarrow \text{stack} \left[A, \text{Im} \left[F_{i_0} \cdot \begin{bmatrix} 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} & 0 \\ 0 & 1 & 0 & -(\omega_{i_0})^2 & 0 & i \cdot \omega_{i_0} \end{bmatrix} \right] \right] \\ \text{for } i \in i_0 + 1 \dots i_f \\ \quad \left| \begin{array}{l} A \leftarrow \text{stack} \left[A, \text{Re} \left[F_i \cdot \begin{bmatrix} 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i & 0 \\ 0 & 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i \end{bmatrix} \right] \right] \\ A \leftarrow \text{stack} \left[A, \text{Im} \left[F_i \cdot \begin{bmatrix} 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i & 0 \\ 0 & 1 & 0 & -(\omega_i)^2 & 0 & i \cdot \omega_i \end{bmatrix} \right] \right] \end{array} \right. \\ A \end{array} \right|$$

<= A = real part of the first frequency
 <= stacks what was on A with the imaginary part of the first frequency
 <= for loop from the second to the last frequencies.
 <= stacks to A the real part of the i^{th} frequency
 <= stacks to A the imaginary part of the i^{th} frequency
 <= returns the matrix A

Auxiliary matrix of zeros [2x2]: $\text{zero}_{1,1} := 0$

The right hand side of the equation is given by:

$$I := \left| \begin{array}{l} I \leftarrow \text{identity}(2) \\ I \leftarrow \text{stack}(I, \text{zero}) \\ \text{for } i \in i_0 + 1 \dots i_f \\ \quad \left| \begin{array}{l} I \leftarrow \text{stack}(I, \text{identity}(2)) \\ I \leftarrow \text{stack}(I, \text{zero}) \end{array} \right. \\ I \end{array} \right|$$

The least squares solution of the problem (minimum E) is: $\underline{\underline{A}} := a(F)$ <= Matrix A for the measured flexibilities

$$q_1 := (A^T \cdot A)^{-1} \cdot A^T \cdot I$$

$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := q_1$$

$$q_1 = \begin{pmatrix} 2.01 \times 10^7 & -10 \times 10^6 \\ -9.99 \times 10^6 & 1.01 \times 10^7 \\ 101.92 & 1.16 \\ 1.15 & 103.13 \\ 4365.36 & -2434.94 \\ -2426.08 & 2447.98 \end{pmatrix}$$

Estimated
system parameters
based on least
squares fit
to flexibilities

$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := \begin{pmatrix} 2 \cdot 10^7 & -1 \cdot 10^7 \\ -1 \cdot 10^7 & 1 \cdot 10^7 \\ 100 & 0 \\ 0 & 100 \\ 4500 & -2500 \\ -2500 & 2500 \end{pmatrix}$$

Actual values:

3. Instrumental variable method



$$q = \begin{pmatrix} 2 \times 10^7 & -10 \times 10^6 \\ -10 \times 10^6 & 1 \times 10^7 \\ 101.9 & 1.1 \\ 1.1 & 103.1 \\ 4366.4 & -2435.6 \\ -2426.8 & 2448.5 \end{pmatrix}$$

Actual values:

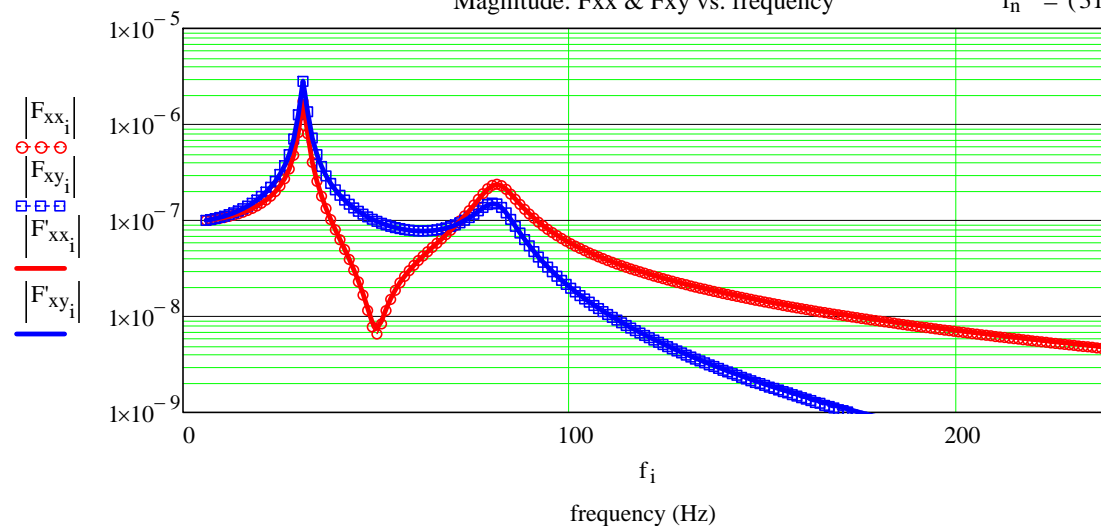
$$\begin{pmatrix} k_{xx} & k_{xy} \\ k_{yx} & k_{yy} \\ m_{xx} & m_{xy} \\ m_{yx} & m_{yy} \\ c_{xx} & c_{xy} \\ c_{yx} & c_{yy} \end{pmatrix} := \begin{pmatrix} 2 \cdot 10^7 & -1 \cdot 10^7 \\ -1 \cdot 10^7 & 1 \cdot 10^7 \\ 100 & 0 \\ 0 & 100 \\ 4500 & -2500 \\ -2500 & 2500 \end{pmatrix}$$

4. Build output/input (transfer functions)



Magnitude: Fxx & Fxy vs. frequency

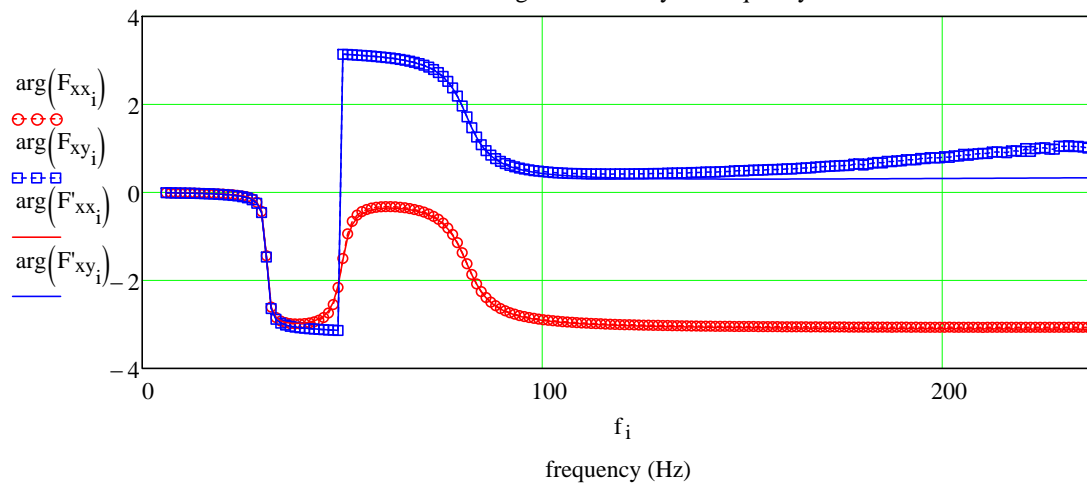
$f_n^T = (31.08 \ 81.13) \text{ Hz}$



SYMBOLS DATA
LINES IVF results

- $\circ \circ \circ$ Fxx (data)
- $\square \square \square$ Fxy (data)
- Fxx (IVF)
- Fxy (IVF)

Phase angle: Fxx & Fxy vs frequency



- $\circ \circ \circ$ Fxx (data)
- $\square \square \square$ Fxy (data)
- Fxx (IVF)
- Fxy (IVF)

